

Frequency of diagnostic tests in practice

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Abstract. The elaboration concerns methods of determination of term of technical equipment next diagnostication. The purpose of it is presentation of three methods related with determination of time of the next examination of equipment state for needs of devices operating system according to technical state.

1 Introduction

During operation the machines' user, on the strength of achieved information on their technical state, creates rules of maintenance them in the state of ability.

Such strategy of operation is called as an operational strategy according to technical conditions. Indispensable elements of this strategy are methods, procedures and means of technical diagnostics, which enable realisation of three essential elements of diagnostic examinations of devices:

- examination and appreciation of devices' technical condition,
- localisation of occurred damages,
- prediction of state changes (forecasting of reliable operation time).

To carry out those examinations, the user should dispose of a set of appropriate procedures: procedure of state control DKS, of damage localisation DLU and of state forecasting.

In case of procedures of state control and damage localisation there is accessible a rich literature in form of manuals (manufacturer's editions) or in form of technological processes of diagnostics (user's trade editions).

For needs of strategy of machines operation according to the technical state, there have been worked out three different methods of determination of term of the next diagnostic examination (for their reliable operation), manner of determination of which is presented in this elaboration.

2 The problem characteristics

The strategy of operation according to the technical conditions is based on making operational decisions on the strength of current estimation of technical state of machines, their assemblies, or parts (fig.1).

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The current machine's technical state, modelled by values of measured state symptoms, is the basis of the operational decision. Correct realisation of this strategy requires using of efficient methods and means of the technical diagnostics as well as trained technical personnel. It also requires overcoming of decision-makers' mistrust concerning effectiveness of such manner of operation. Economic effects of such operational manner are incommensurably higher than in other strategies, what ensures success and great interest of this solution.

The basic condition of this strategy success is accessibility of simple and effective diagnostic methods, best of all incorporated in manufactured machines, which are then supervised in a system of the state monitoring.

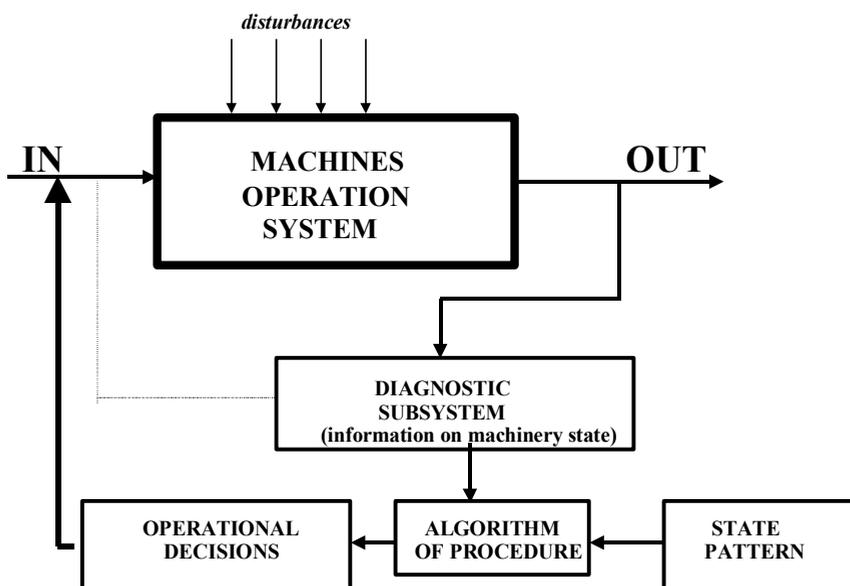


Fig.1. Diagnostic control of machines operation system

Based on known strategies of machines operation [4], in industrial practice there are built systems of machines' technical operations. Among the most spread ones we can find:

- system of prophylactic changes built mainly on the strength of operational strategy according to activity; (for single reliable objects - where prophylactic changes are carried out to avoid failure)
- according to a fixed plan - preventive system of technical operations; built based on strategy according to amount of performed work; (in advance planned range and frequency of technical operations, independently on current state, that is needs),
- according to a fixed plan - preventive system of technical operations with diagnostics; (like above, but helped by partial diagnostics of machine's state),
- system of technical operations according to the state; (servicing activities - frequency and range - are determined based on current machine's technical state).

Some of the basic problems of technical operations system according to technical state is the need of knowledge of the way of determination of the next term of state diagnostics, determined depending on current values of measured state symptoms.

Let phenomenon of devices' technical state destruction is represented by the time series $S_t = \langle s_1, s_2, s_3, \dots, s_b \rangle$, it means by the set of discrete observations $\{St = \zeta(\Theta); \Theta = \Theta_1, \Theta_2, \dots, \Theta_b\}$ of any unsteady stochastic process $\zeta(\Theta)$. With assumption, that mechanism of changes of stochastic process values in time $t \in (\Theta_1, \Theta_b)$ is shaped by the trend $\mu(\Theta)$ disturbed by various random interactions $\eta(\Theta)$:

$$y_t = \mu(\Theta) + \eta(\Theta) \quad (1)$$

where:

$\mu(\Theta)$ - characterises a determined component of the time series y_t ; it describes a developmental tendency of observed diagnostic parameter $S(\Theta)$,

$\eta(\Theta)$ - characterises aberrations from the trend and expresses effects of accidental parameters (ground and climate conditions, quality of maintenance);

there is also constructed an estimation $\{\mu_p(\Theta); t = 1, 2, \dots, b\}$ for unknown form of the trend $\mu(\Theta)$, which would ensure an appropriate accuracy of forecast $S_p(t)$, with extrapolation $\mu_p(\Theta)$ for time interval of devices usage (mileage) (Θ_b, Θ_p) , where: $\Theta_p = \Theta_b + \tau$.

As permissible period of usage (time of reliable operation) there is accepted the time, in which limits of error interval for individual forecast:

$$\sigma(S_t, S_p, P(S_t, \tau)) \quad (2)$$

determined on a subset $\Omega_y \subset \Omega$ of accessible realisations of observed parameters $\{S_j(\Theta)\}$ as well as of forecasts of them $\{S_j, p\}$ according to accepted predictor $P(S_t, \tau)$, do not exceed limiting values $\{S_j, gr\}$.

Value of permissible time of device's reliable operation determines the temporal horizon of a forecast $\tau_j^0 [1, 2]$:

a) for which there will not be observed any exceeding of limiting value of diagnostic parameter S_j, gr by the limit of the forecast error interval determined by the radius $r\sigma$ (method of forecast error value levelling):

$$r\sigma = q\sigma_p \quad (3)$$

where:

q - is a stable parameter calculated from the student's distribution table for required confidence level γ and $K-2$ numbers of degree of freedom,

σ_p - standard deviation of a random component of forecast error ep .

b) for which there will not be observed any exceeding of limiting value of diagnostic parameter S_j, gr by forecasting value of diagnostic parameters (method of diagnostic parameter limiting value levelling),

c) for which there will not be observed any exceeding of limiting value of diagnostic parameter S_j, gr by measured value of diagnostic parameter (method of diagnostic parameter change estimation).

3 Method of determination of reliable operation time by means of forecast error value levelling

In case of strategy of operation according to technical state, a required form of the devices' state forecast PST is the term of the next diagnostics Θ_{b1} :

$$PST = \langle \Theta_{b1}, \rangle \quad (4)$$

As the value Θ_{b1} it is proposed to accept a value of permissible device reliable operation time, determined by a value of horizon τ_j^0 , fixed as a point of intersection of a line of diagnostic parameter limiting value S_j, gr with the bottom (with assumption that $S_j(\Theta_b) > S_j, gr$) or upper

(with assumption that $S_j(\Theta_b) < S_{j,gr}$) limit of forecast error interval (fig.2) determined by radius $r\sigma$ for two confidence coefficients:

- a) $r\sigma_{0,01}$ for confidence level $1 - \gamma = 0,99$, what responds to probability of value $p=0,01$, where in the interval determined by a horizon τ_j^* a diagnostic parameter S_j achieves a limiting value $S_{j,gr}$;
- b) $r\sigma_{0,05}$ for confidence level $1 - \gamma = 0,95$, what responds to probability of value $p=0,05$, where in the interval determined by a horizon τ_j^{**} a diagnostic parameter S_j achieves a limiting value $S_{j,gr}$.

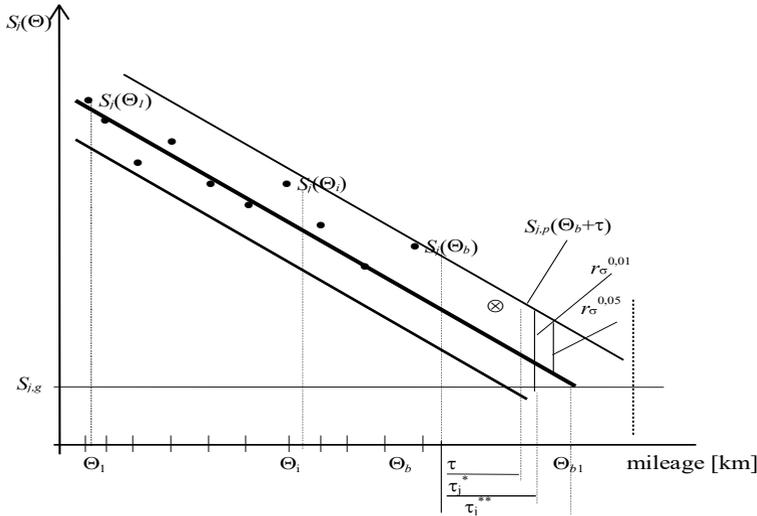


Fig.2. Determination of the term of the next devices diognostication Θ_{b1} by means of the method of forecast error value levelling for $S_j(\Theta_b) > S_{j,gr}$. [Θ_1 - the beginning of device operation, Θ_b - the last device diognostication, Θ_{b1} - the term of the next device diognostication].

Three options are then distinguished:

- a) not exceeding by a controlled diagnostic parameter of a limit determined by a radius $r\sigma_{0,01}$ is interpreted as a lack of alarm signal for careful and more exact diagnostic observation of the device;
- b) exceeding by a controlled diagnostic parameter of a limit determined by a radius $r\sigma_{0,01}$ is interpreted as an alarm signal for careful and more exact diagnostic observation of the device (alert threshold);
- c) moment of exceeding by a controlled diagnostic parameter of a limit determined by a radius $r\sigma_{0,05}$ is interpreted as the time Θ_{b1} - the term of the next device diognostication (alarm threshold).

Values $S_{j,p}(\Theta_b + \tau)$ and Θ_{b1} , with assumption that the Brown-Mayer's method of the first order is an optimal method of forecasting, are calculated according to expressions:

$$S_{j,p}(\Theta_b + \tau) = at(0) + \tau at(1) \tag{5}$$

where:

$$at(0) = Mt = 2Mt(1) - Mt(2)$$

$$at(1) = Tt = \frac{\alpha}{(1-\alpha)} (Mt(1) - Mt(2))$$

and:

$$Mt(1) = \alpha y_t + (1 - \alpha) Mt-1(1)$$

$$\begin{aligned}
 & Mt(2) = \alpha Mt(1) + (1 - \alpha) Mt(1)(2) \\
 & \alpha - \text{parameter of exponential smoothing, } \alpha \in (0,1) \\
 & \Theta_{b1} = \Theta_b + \frac{\tau (S_j(\Theta_b) - r_\sigma)}{S_j(\Theta_b) - S_{j,p}(\Theta_b + \tau)} \quad (6)
 \end{aligned}$$

The time interval (Θ_1, Θ_b) will then be a period of estimation of forecast error value ϵ_p and radius r_σ , whilst the time interval after Θ_b will be a period of active forecasting, i.e.:
 a) determination of forecasting value of diagnostic parameter after time τ , $S_{j,p}(\Theta_b + \tau)$;
 b) determination of a radius $r_\sigma(\Theta_b + \tau)$ value;
 c) determination of the term of the next device diagnostics Θ_{b1} .

4 Method of determination of the time of reliable operation by means of levelling of diagnostic parameter limiting value

In this method as a term of the next device diagnostics Θ_{b1} is proposed to accept a value of permissible time of device reliable operation, determined by a horizon value τ_{j0} , fixed as a point of intersection of lines (fig.3) of diagnostic parameter value S_j with:

a) lower (with assumption, that $S_j(\Theta_b) > S_{j,gr}$) limit for two levels of limiting values:

$$\begin{aligned}
 S_{j,gr}^* &= \frac{2}{10} |S(\Theta_1) - S_{j,gr}| + S_{j,gr} \quad (7) \\
 S_{j,gr}^{**} &= \frac{1}{10} |S(\Theta_1) - S_{j,gr}| + S_{j,gr}
 \end{aligned}$$

b) or upper (with assumption, that $S_j(\Theta_b) < S_{j,gr}$) limit determined for two levels of limiting values:

$$\begin{aligned}
 S_{j,gr}^* &= S_{j,gr} - \frac{2}{10} |S(\Theta_1) - S_{j,gr}| \quad (8) \\
 S_{j,gr}^{**} &= S_{j,gr} - \frac{1}{10} |S(\Theta_1) - S_{j,gr}|
 \end{aligned}$$

Values $S_{j,p}(\Theta_b + \tau)$ and Θ_{b1} , with assumption that the Brown-Mayer's method of the second order is an optimal method of forecasting, are calculated according to expressions:

$$S_{j,p}(\Theta_b + \tau) = at(0) + \tau at(1) + \tau^2 at(2) \quad (9)$$

where:

$$\begin{aligned}
 a_t^{(0)} &= M_t = 3(M_t^{(1)} - M_t^{(2)}) + M_t^{(3)} \\
 a_t^{(1)} = T_t &= \frac{\alpha}{2(1-\alpha)^2} \left\{ (6-5\alpha) M_t^{(1)} - 2(5-4\alpha) M_t^{(2)} + (4 - 3\alpha) M_t^{(3)} \right\}
 \end{aligned}$$

$$a_t^{(2)} = Q_t = \frac{\alpha^2}{2(1-\alpha)^2} \left\{ M_t^{(1)} - 2M_t^{(2)} + M_t^{(3)} \right\}$$

$$\begin{aligned}
 M_t^{(1)} &= \alpha y_t + (1 - \alpha) M_{t-1}^{(1)} \\
 M_t^{(2)} &= \alpha M_t^{(1)} + (1 - \alpha) M_{t-1}^{(2)} \\
 M_t^{(3)} &= \alpha M_t^{(2)} + (1 - \alpha) M_{t-1}^{(3)}
 \end{aligned}$$

α - parameter of exponential smoothing, $\alpha \in (0,1)$

$$\Theta_{b1} = \Theta_b + \frac{\tau (S_{j,g}^{**} - S_j(\Theta_b))}{S_j(\Theta_b + t) - S_j(\Theta_b)} \quad (10)$$

Making n - measurements of a signal measure, chosen in separate procedure, it is possible to determine, based on it, the limiting value, depending on the relationship:

$$S_{jgr} = s + \sigma_s \sqrt{\frac{P_g}{2A}}, [P_g - \text{repairing policy of the Works}],$$

$$A = k(1 - P_g), k = \{1-9\} \tag{11}$$

and then determine the term of the next diagnostics Θ_{b1} according to above proposed procedure.

Probability P_r of failure-free machine's work is determined by the ratio of number of machines N_k without damages with $S_j < S_{jgr}$ within inter-inspections period to machines' number N_p based on considered [period of work. The number of machines with damages ($S_j > S_{jgr}$) w in assigned period of time amounts:

$$n = N_p - N_k$$

and adequately: $P_r = 1 - n / N_p$ (12)

The number of machines revealing n -failures within inter-revisions period, in relation to number of S_{jgr} exceeding amounts

$$n = N_{sr} [S(\Theta_i) \Theta_{b1}] \tag{13}$$

where: $N_{sr} = (N_p + N_k) / 2$; Θ_{b1} - time of the next diagnostics (km, hour); $S(\Theta_i)$ - parameter characterising an ascending dynamic for symptomatic curve of life in considered period Θ_j , defined according to relationship:

$$S(\Theta_i) = \left(\frac{S_j}{S_{jgr} - S_j} \right) \left(\frac{1}{\Theta_j} \right) [1/\text{km, godz}] \tag{14}$$

where: S_j - value of measured symptom, S_{jgr} - limiting value of the symptom.

Providing (13) to (12) after transformation we obtain following relationships:

$$P_r = \frac{2 - S(\Theta_i) \cdot \Theta_{b1}}{2 + S(\Theta_i) \cdot \Theta_{b1}}$$

$$\Theta_{b1} = \frac{2(1 - P_r)}{S(\Theta_i)(1 + P_r)} \tag{15}$$

With exponential syndrome distribution in time Θ_j the above equations assume following form:

$$P_r = e^{-S(\Theta_i)\Theta_{b1}}$$

$$\Theta_{b1} = \frac{-\ln P_r}{S(\Theta_i)} \tag{16}$$

Assuming $1 < P_r < 0,8$ with an accuracy sufficient for practice one may use an approximate expression:

$$P_r = 1 - S(\Theta_i) \Theta_{b1} \tag{17}$$

Assuming constant intensity of symptomatic curve of life ascending (assigned P_r) we achieve:

$$P_r = \text{const} \quad \text{thus} \quad S(\Theta_i) \Theta_{b1} = \text{const} \tag{18}$$

From which it results that the higher $S(\Theta_i)$ the smaller Θ_{b1} , what in interpretation of symptomatic diagnostics means, that as a symptom increase (approaching to S_{jgr}) within machine's time-life Θ_j , diagnostics frequency increases (fig.4).

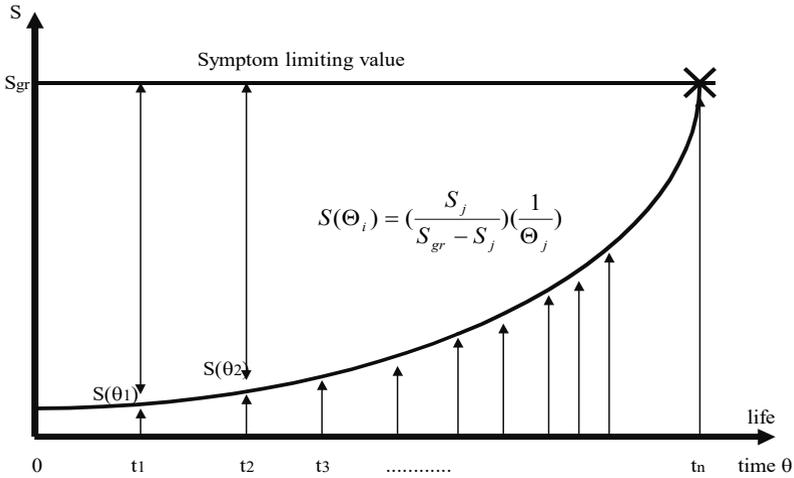


Fig.4. Periodicity of diagnostication in symptomatic depiction.

From the relationship (17) one may thus determine Θ_{b1} :

$$\Theta_{b1} = \frac{1 - P_r}{S(\Theta_i)} \text{ and after providing a relationship (14)}$$

finally:

$$\theta_{b1} = \frac{(1 - P_r)(S_{gr} - S_j)}{S_j} \Theta_j \tag{19}$$

Presented relationship allows to determine the term of the next diagnostication in relation to current value of measured symptom, its relation to symptom's limiting value and with considering the repairing policy of the works [3,4].

6. Conclusions

In this elaboration there are presented three methods of determination of devices reliable operation time in form of the term of the next technical equipment diagnostication for needs of strategy of operation based on technical state:

- a) by means of forecast error value levelling,
- b) by means of levelling of diagnostic parameter limiting value,
- c) by means of diagnostic parameter change estimation.

Carried out verifying examinations of efficiency of proposed methods reveal some limitations and preferences in their practical application.

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