

THE PROJECT “PARSIFAL”: PRANDTLPLANE ARCHITECTURE FOR THE SUSTAINABLE IMPROVEMENT OF FUTURE AIRPLANES

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Abstract. The activities reported in this paper are part of the project “PARSIFAL” (PrandtlPlane ARchitecture for the Sustainable Improvement of Future AirpLanes), funded by the European Community under the Horizon 2020 program and coordinated by the University of Pisa (Italy); the other partners of the project are: Delft University of Technology (The Netherlands), ONERA (France), Arts et Métiers ParisTech-ENSAM (France), DLR (Germany) and SkyBox Engineering (Italy). The paper presents a summary of preliminary design activities, carried out with the project PARSIFAL in order to study the introduction of box-wing aircraft, known as “PrandtlPlane”, in the air transport system. PARSIFAL aims to investigate the adoption of the PrandtlPlane over short-to-medium routes, where aircraft compliant with the ICAO Aerodrome Reference Code “C” operate. According to such ICAO standard, the PrandtlPlane developed in PARSIFAL has a wingspan limited to 36m but, if compared to reference aircraft such as B737 and A320 families aircraft, it can improve the passenger capacity from about 200 to more than 300 units. This paper presents the design steps performed for the definition of a “baseline configuration” of the PrP, introducing the requirements and describing both the conceptual and preliminary design phases, including the high fidelity investigations CFD and FEM analyses.

1 Introduction

According to several European studies ([1, 2, 3]), novel aircraft configurations as the ones shown in Fig. 1 represent one of the possible way to achieve the following:

- to fulfil the growth of air traffic demand, which is expected to double in next 20 years;
- to reduce CO₂ and NO_x emissions and noise per passenger-kilometres;
- to reduce to 4 hours the time required for a door-to-door journey within Europe.

The story of the box-wing configuration called “PrandtlPlane”, or PrP (Fig. 1-right), has started in in 1924 when Ludwig Prandtl found that the so-called “best wing system” (BWS) has the property of minimizing the induced drag for given lift and wingspan ([4]). In 1990s, research performed at Pisa University have shown that a closed-form-solution of the minimum induced drag problem exists ([5]) and that it is possible to apply the Prandtl’s concept to aircraft design ([6, 7, 8, 9, 10, 11]).

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Fig. 1. Three examples of novel aircraft configurations. From left to right: the blended wing body (BWB), the truss-braced wings (TBW) and the box-wing or “PrandtlPlane” (PrP)

The present paper deals with the application of the PrP concept to commercial flight, in the framework of the EU funded project PARSIFAL (“Prandtlplane ARchitecture for the Sustainable Improvement of Future AirPLanes”), in which the future challenges of air transport are faced exploiting the aerodynamic advantages of the box-wing through the improvement of payload capabilities without increasing the overall dimensions of the aircraft.

1.1 Top Level Aircraft Requirements

The requirements adopted in PARSIFAL for the PrP design have been defined starting from the analysis of air traffic demand forecasts for 2030s, in which short-to-medium routes (<4000 km) will see the higher growth rate.

Today short-to-medium routes are flown mainly by single aisle aircraft with about 200 passengers, such as aircraft from Airbus 320 or Boeing 737 families. Therefore, in order to make use of the same airport infrastructures, the wingspan of the PrP has been limited to 36 m, introducing the compliance with ICAO Aerodrome Reference Code “C” specification as a requirement. The choice of such aircraft category brings a set of constraints and typical mission parameters, which are summarized in the following Top-Level Aircraft Requirements (TLARs):

- number of passengers between 250 and 320 (high density),
- maximum range covered with maximum number of passengers of 2160 NM (4000 km),
- compliance with the ICAO Aerodrome Reference Code “4C” (“4” indicates a Take-Off Field Length > 1800m, whereas “C” refers to a wingspan < 36m and wheel span between 6m and 9m),
- initial cruise altitude of 36000ft,
- Mach number in cruise flight greater than or equal to 0.78.

2 Conceptual design of the PrandtlPlane

The conceptual design of the PrP has been performed considering the aforementioned TLARs, focusing the efforts on the fuselage and the box-wing system.

As detailed in [12] and [13], the TLARs have been first used for the conceptual design of the fuselage, for which a single deck - double aisle layout with 8 seats abreast has been chosen. As a result, a 44 m long fuselage with a maximum payload capability of 308 seats in high density configuration and 12 LD3-45 containers have been defined (Fig. 2).

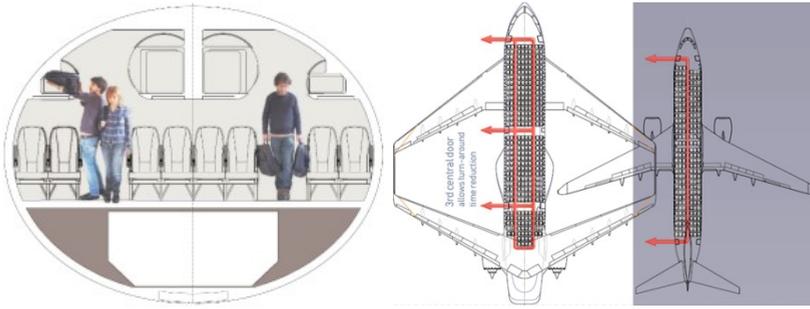


Fig. 2. Conceptual design of PrandtlPlane's fuselage and cabin

The conceptual design has been completed defining the box-wing design space, which has been explored by means of an optimization in-house developed tool, called AEROSTATE, which is based on the Vortex-Lattice Method (VLM) code AVL.

The optimization problem used for the PrP conceptual design is:

$$\begin{aligned}
 &\min [-L/D(\mathbf{x})] \\
 &g(\mathbf{x}) \geq 0 \\
 &h(\mathbf{x}) = 0 \\
 &lb < \mathbf{x} < ub
 \end{aligned}
 \tag{1}$$

where \mathbf{x} is the vector of design parameters, each of them bounded in a specific interval (l_b , u_b), the objective function is related to lift-to-drag ratio (L/D) in cruise condition, whereas $g(\mathbf{x})$ and $h(\mathbf{x})$ are constraint functions which take flight mechanics (e.g.: trim, longitudinal stability), aerodynamics (e.g.: lift distributions) and several geometric constraints into account.

At the end of the optimization process, AEROSTATE provide a set of feasible solutions white different values of L/D (Fig. 3).

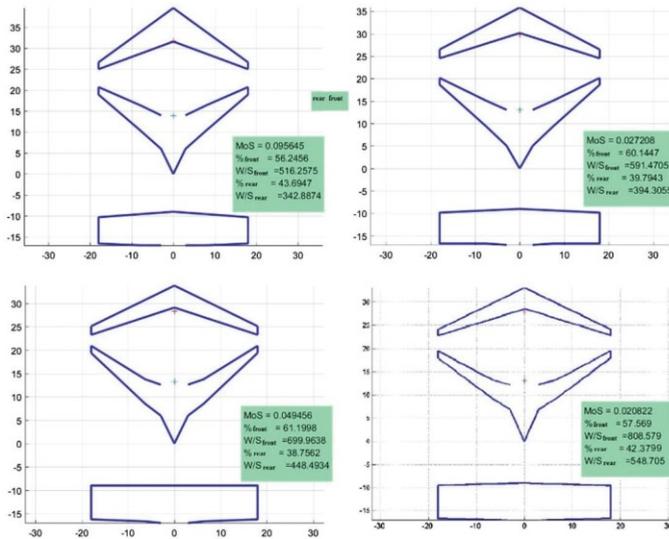


Fig. 3. Example of set of solutions provided by AEROSTATE

3 High fidelity investigations

3.1 Aerodynamics

From the early stages of the project, it was necessary to investigate the aerodynamic behaviour of the PrP in cruise conditions with high-fidelity CFD tools. Such activity has been focused mainly on the effects of a set of design variables, such as the wing loading and geometric parameters, on transonic aerodynamics.

Test case configurations have been designed using AEROSTATE and Mach contours in cruise, as the ones shown in Fig. 4, have been investigated.

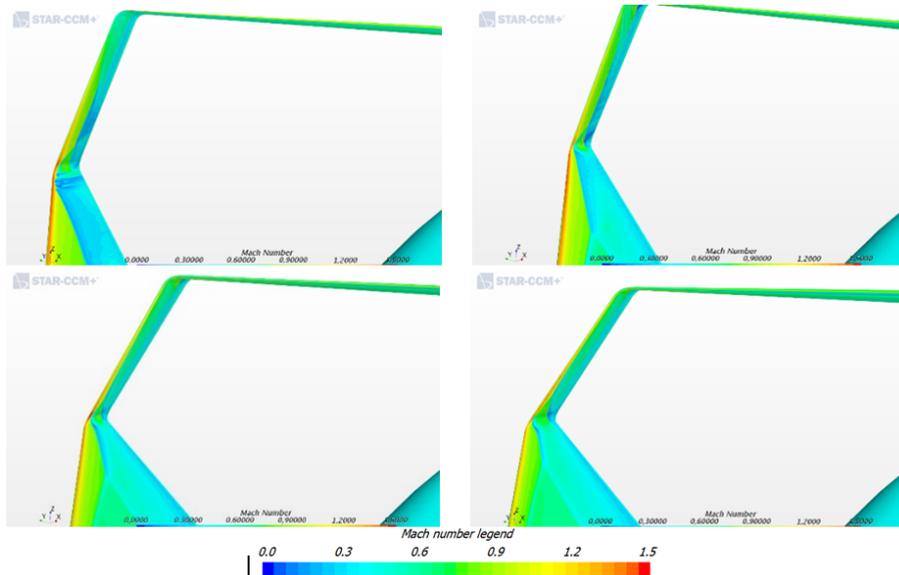


Fig. 4. Maps of local Mach number obtained through CFD simulations for different test case configurations

As described in [13], a trade-off between the performance in subsonic and transonic conditions is needed: in the first case, in fact, higher values of lift-to-drag ratio are achievable only considering higher values of wing loading ([13, 15]), whereas in transonic flight, high values of wing loading can lead to drag rise conditions.

Information obtained from such CFD campaign has been used to properly calibrate the constraints and the boundaries of the AEROSTATE code, which is based on a potential aerodynamic solver, and so is not able to provide information on the compressibility effects on the drag in transonic flight.

Other investigations on geometric parameters' effects have been performed in order to improve the local aerodynamic performance, removing or limiting increases of drag due to the presence of shock waves.

3.2 Structures

Preliminary structural sizing has been performed with an in-house pre-processing tool, called WAGNER ([16, 17]), and commercial FEM software. Although it can be used for any aircraft configuration, WAGNER has been adopted in order to create detailed general FE model of PrP main structures, including stringers, frames, ribs, pressurization bulkheads, floor beams and floor struts (Fig. 5).

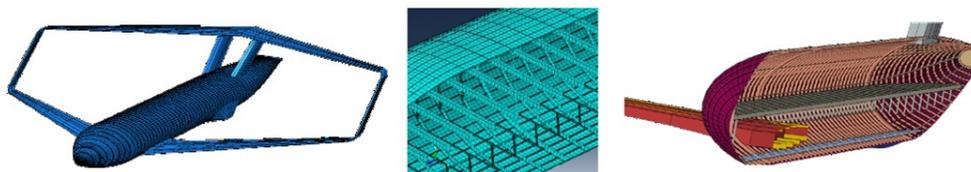


Fig. 5. Qualitative pictures of models generated by WAGNER

WAGNER has been used from the early stages of the project, in order to predict the total structural weight and CG position of the configuration, considering both aerodynamic and pressurization loads, under the main hypothesis of linear, homogeneous and isotropic elastic materials, which is suitable for metallic structures.

3.3 Flight Mechanics

Since there are different possible solutions to control and maneuver a PrP aircraft, in the initial phase of the project a reference layout has been selected: counter-rotating elevators are installed in the front and rear wing-root regions, ailerons are installed at the tip of each lifting surface, whereas high-lift devices are positioned in the reaming central region of each wing (Fig. 6).

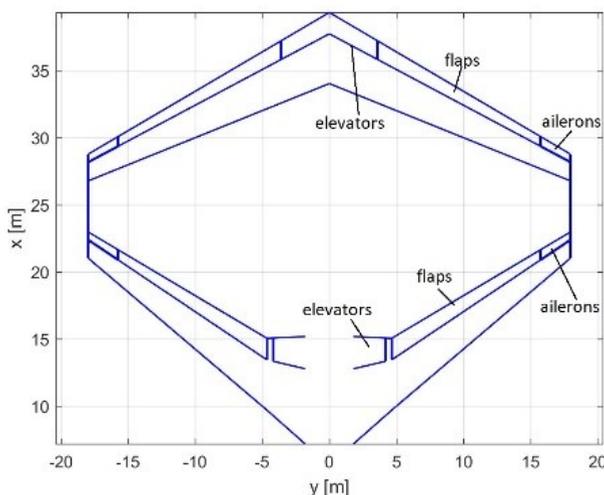


Fig. 6. Reference layout for PrP control surfaces

A VLM-based procedure for the preliminary sizing of control surfaces and high-lift devices has been defined for the PrP, considering the trim constraints in approach condition, as described in [13]. Such procedure results in an initial sizing of the control surfaces, and a preliminary estimation of the low speed performance of the aircraft, together with its aeromechanical characteristics of maneuverability and control.

Such information have been then used as input for higher fidelity assessments, in which CFD analyses have been performed to refine the evaluation of control derivatives. The pressure coefficient maps shown in Fig. 7 represent some of the obtained results, which have provided information useful to assess the behavior of this control systems layout, but also to validate or calibrate lower fidelity methodologies.

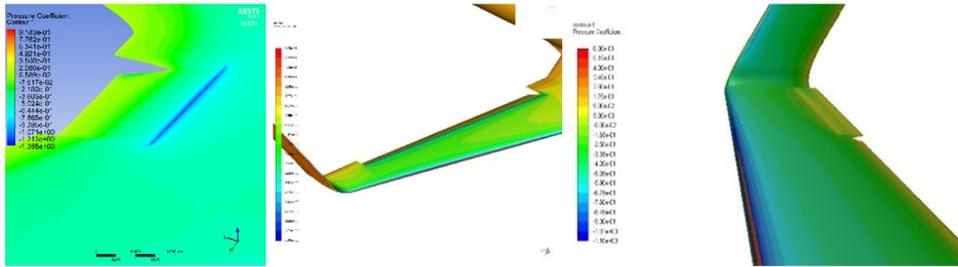


Fig. 7. Cp maps in approach condition for the PrP front wing with deflected elevator (left), flap (middle) and aileron (right)

4 The Baseline PrP configuration

The preliminary design phase has started from the outcomes of the high fidelity investigations and, taking further aspects into account, such as landing gear design ([18]) and take-off performance analysis ([19]), has ended up in the definition of a baseline PrP configuration, which is briefly described in Table 1.

Table 1. Characteristics of the baseline PrP configuration

Design conditions	
N. Passengers (high density)	310
Flight Altitude [m]	11000
Flight Speed [m/s]	233
Cruise Mach	0.79
Aircraft data	
Wing Area (front + rear) [m ²]	267
Wingspan (incl. winglets) [m]	36
Fuselage Width [m]	5.40
Fuselage Length [m]	44
MTOW [tons]	122
Take-off Thrust per engine [kN]	180

The baseline PrP has an important role in PARSIFAL, since it is not only the starting point for the advanced design loop, but it represents the reference configuration for assessing the impact assessment of the introduction of the PrP as a mean of transport.

Since one of the main drivers for the environmental and economic impact of an aircraft is the fuel consumption, the aerodynamic efficiency of the baseline PrP has been evaluated through CFD models ([20]). Considering a flight program with constant altitude ($h=11000\text{m}$) and Mach ($M=0.79$), the whole cruising phase has been simulated calculating:

- the fuel flow, i.e. the fuel burnt by each engine per unit time ;
- the thrust required to each engine;
- the total fuel burnt as the time-integral of fuel flow multiplied by the number of engines.

5 Conclusions and further development

The project PARSIFAL has come its final phase, in which the PrP designed to improve the payload capability of aircraft with wingspan below 36 m, such as A320 and B737,

while keeping the compatibility with present airport infrastructures, is under investigation from the standpoint of impact assessment.

The PrP considered is the one resulting from the 1st design loop, which has started taking a set of Top Level Aircraft Requirements defined with a market-oriented approach into account. The paper, hence, has described both the conceptual design phase, in which the fuselage and the box-wing system have been object of low-fidelity studies, and the preliminary design.

Next steps of the research will be focused on the further development of the PrP configuration. The results of such activities will provide the input for the 2nd design loop, which aims to provide an updated version of the PrP, which will be assessed in terms of environmental, logistic and economic impact.

6 Acknowledgments

The present paper concerns part of the activities carried out within the research project PARSIFAL (“Prandtlplane ARchitecture for the Sustainable Improvement of Future AirPLanes”), which has been funded by the European Union under the Horizon 2020 Research and Innovation Program (Grant Agreement n.723149).

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