

Parametric Study on Vibration and Harmonic Analysis of Moderately Thick Functionally Graded Plates Using FEM

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Abstract. Finite element method is used to investigate the free vibration and harmonic analysis of functionally graded plates. The material properties of the plates are assumed to vary continuously through their thickness direction according to a power-law distribution of the volume fractions of the plate constituents. The four noded shell 181 elements are used to analyse the functionally graded plates. The aim is to fill the void in the available literature with respect to the free vibration results of Functionally Graded plates. Convergence and Comparison studies with respect to the number of nodes has been carried out using FEM. The natural frequency, mode shape and harmonic analysis of FG plate has been determined using finite element package ANSYS.

1. Introduction

Composite materials have been widely used in aircraft and other engineering applications for many years because of their excellent strength-to-weight and stiffness-to-weight ratios. Functionally graded materials (FGM) are a class of composite materials that were first proposed by Bever and Duwez [1] in 1972. In a typical FGM plate the material properties continuously vary over the thickness direction by mixing two different materials [2], usually ceramic and metal. The gradual variation of properties avoids the delamination failure that are common in laminated composites. The computational modelling of FGM is an important tool to the understanding of the structures behavior, and has been the target of intense research, from micro to macro mechanics [3–6]. Researchers have also turned their attention to the vibration and dynamic response of functionally graded structures [7–9]. Sheng and Wang [10] investigated the effect of thermal load on vibration, buckling and dynamic stability of functionally graded cylindrical shells embedded in an elastic medium. A review of the main developments in FGM can be found in Birman and Byrd [11]. Sharma et. al. [12] presented the free vibration of shear-deformable antisymmetric angle-ply laminated rectangular plates having translational as well as rotational edge constraints. The Vibration attenuation using functionally graded material is studied by Saeed et. al. [13].

The vibration and harmonic responses of composite plates and FGMs have been extensively studied by a number of researchers [14-16]. However, the aim of the work is to study the effect of functionally graded materials on the vibration behaviour by doing modal and harmonic analysis of the models.

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2. Functionally Graded Material Properties

A functionally graded material plate as shown in fig. 1 is considered to be a plate of uniform thickness that is made of ceramic and metal. The material property is assumed to be graded through the thickness according to a Power-Law distribution that is

$$P(z) = (P_c - P_m)V_m + P_m \quad (1)$$

where P_m , P_c , V_m and V_c are the material properties and the volume fraction of the metal and ceramic, respectively, the compositions represent in relation to

$$V_c + V_m = 1 \quad (2)$$

The volume fraction of ceramic (V_c) can then be written as follows:

$$V_c = \left(\frac{z}{h} + \frac{1}{2} \right)^n \quad (n \geq 0) \quad (3)$$

where the positive number n ($0 \leq n \leq \infty$) is the power law or the volume fraction index. z is a distance parameter along the graded direction, while, h is the total length of the direction. To find out the results of material properties according to the power law distribution, this can be achieved by substituting the equations of material volume fractions Eq. (2) and Eq. (3) into Eq. (1).

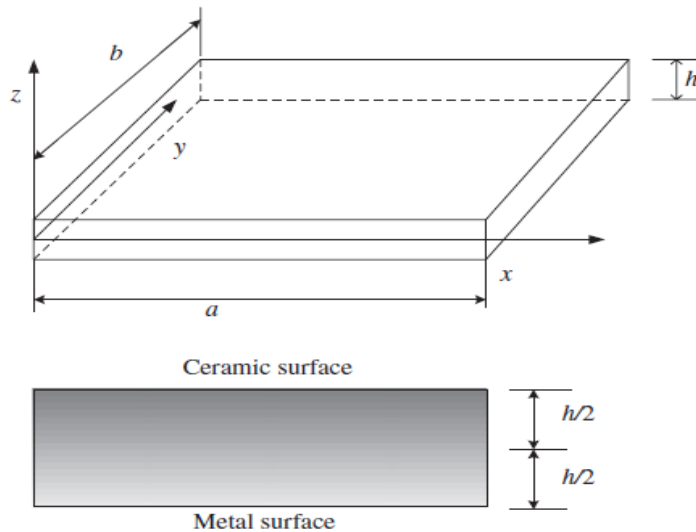


Figure 1. Geometry of Functionally graded plate

3. Results and Discussion

3.1 Modal Analysis

The variation of the frequency parameter with the boundary condition for functionally graded plates is described in Tables 1-2 respectively. It shows a comparison of the fundamental natural frequency parameters of functionally graded plates for volume fraction exponent $n=0$. It can be seen that as the mesh size increases the results are converging and convergence is achieved at the mesh size of 19×19 . The results are compared with the Zhao et. Al. [17].

Table 1: Variation of the frequency parameter with the volume fraction exponent $n=0$ for square FG plates ($a/h = 10$) with CFFF

3x3	11.7174	22.4627	26.6912	33.8398	37.9197	38.1226	42.2459	45.4010	45.7544	51.0061
5x5	10.5809	20.7963	20.9147	29.6169	35.8369	36.0877	37.7263	37.7364	43.2174	44.1762
7x7	10.3100	19.9219	19.9483	28.2032	33.6206	33.8827	37.6205	37.6217	40.7289	40.8631
9x9	10.2299	19.7064	19.7360	27.8315	33.0467	33.3661	37.5852	37.5877	40.0541	40.1108
11x11	10.1758	19.5785	19.5823	27.6009	32.7228	33.0107	37.5606	37.5625	39.6554	39.6894
13x13	10.1512	19.5149	19.5256	27.4901	32.5559	32.8432	37.5486	37.5499	39.4632	39.4701
15x15	10.0340	19.2276	19.2295	27.0157	31.8887	32.2346	37.5341	37.5348	38.6379	38.6492
17x17	10.0006	19.1325	19.1369	26.8727	31.6978	32.0229	37.5260	37.5266	38.3941	38.3985
19x19	9.9918	19.1098	19.1111	26.8317	31.6556	31.9637	37.5215	37.5222	38.3361	38.3412
21x21	9.9830	19.0859	19.0865	26.7914	31.6021	31.9101	37.5171	37.5171	38.2631	38.2649
23x23	9.9666	19.0487	19.0518	26.7429	31.5258	31.8408	37.5089	37.5096	38.1824	38.1887
Zhao et. al [16]	9.6329	18.313	18.313	25.499						

Boundary conditions at different mesh size:

Table 2: Variation of the frequency parameter with the volume fraction exponent $n=0$ for square FG plates ($a/h = 10$) with

3x3	1.077363	2.617083	6.68115	6.6994	8.2656	9.61884	15.98373	16.70256	17.88	19.90044
5x5	1.059282	2.504943	6.292314	6.6389	7.95501	8.95734	15.30396	15.91632	17.56	17.79309
7x7	1.054494	2.489193	6.228243	6.6289	7.86429	8.80803	14.93163	15.90057	17.05	17.77923
9x9	1.0521	2.481381	6.200838	6.6238	7.83846	8.75952	14.81823	15.89175	16.91	17.68851
11x11	1.050777	2.476467	6.18786	6.6213	7.82019	8.73243	14.75334	15.88671	16.84	17.61984
13x13	1.049706	2.472498	6.17778	6.62	7.81074	8.71101	14.70483	15.88419	16.8	17.58204
15x15	1.046745	2.459205	6.142626	6.6182	7.77357	8.64045	14.55552	15.88104	16.62	17.43336
17x17	1.046052	2.457819	6.133995	6.6175	7.76412	8.62974	14.53158	15.87915	16.58	17.40375
19x19	1.045737	2.456937	6.131727	6.6169	7.76223	8.62533	14.52213	15.87789	16.57	17.39241
Zhao et. al [16]	1.0298	2.3907	6.0047	7.6356						

CCCC Boundary conditions at different mesh size:

Table 3: frequency response amplitude of FG square plate with different volume fraction exponent

B.C.	Volume fraction exponent	Mode	Frequency (Hz)	Amplitude (m)
CCCC	$n = 0$	Mode 1	1592.7	0.0000000146726
CCCC	$n = 1$	Mode 1	1324.5	0.0000000247805
CCCC	$n = 5$	Mode 1	858.76	0.0000000699683
CCCC	$n = 10$	Mode 1	811.53	0.0000000793071

3.2 Harmonic Analysis

To know FRF plot, harmonic analysis is to be done by providing the range of natural frequency of 0 Hz to 2000Hz and 100 substeps. It will generate FRF plot (linear) on graph of amplitude to frequency,

frequency (Hz) is taken on the x-axis and amplitude (m) on the y-axis. From this graph we come to know its resonance point. Also many details of system such as amount of displacement, by how much frequency by how much amount system excited. It can be said that the overall response of system can be known. It is clear from the Table 1 that as the volume fraction exponent increases the frequency response amplitude of FG plates increases.

These frequency response amplitudes can also be reduced by providing damping constant. In the study, constant damping ratio of 0.01 is taken. Effect of volume fraction exponent on the frequency response amplitude for different sets of FG plates is shown in Figure 2-5 respectively. It is clear from the figures that as the volume fraction exponent increases the frequency response amplitudes increases. Figure 6 shows the first four modes of functionality graded plates.

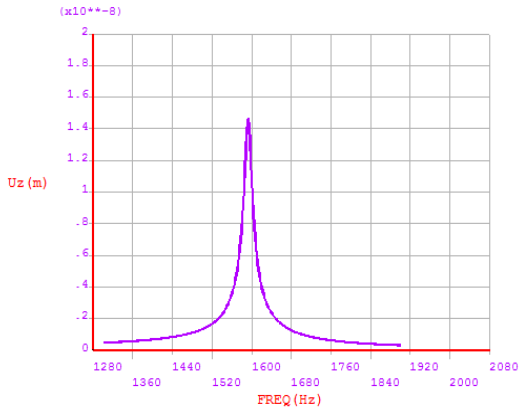


Figure 2. shows the FRF plots without damping FG plate at CCCC boundary condition at $n=0$.

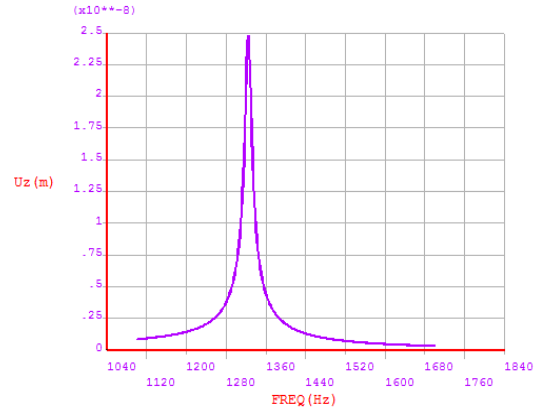


Figure 3. shows the FRF plots without damping FG plate at CCCC boundary condition at $n=1$.

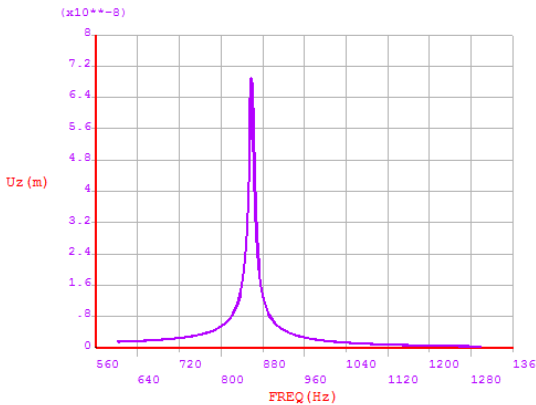


Figure 4. shows the FRF plots without damping FG plate at CCCC boundary condition at $n=5$.

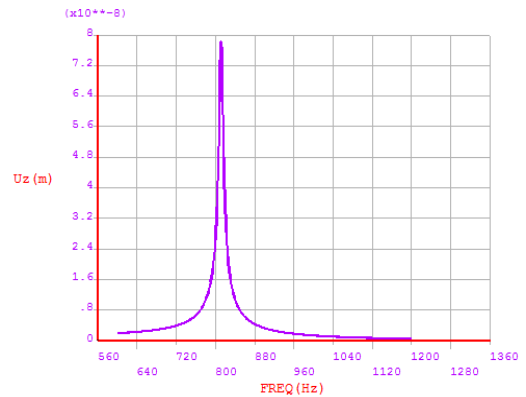


Figure 5. shows the FRF plots without damping FG plate at CCCC boundary condition at $n=10$.

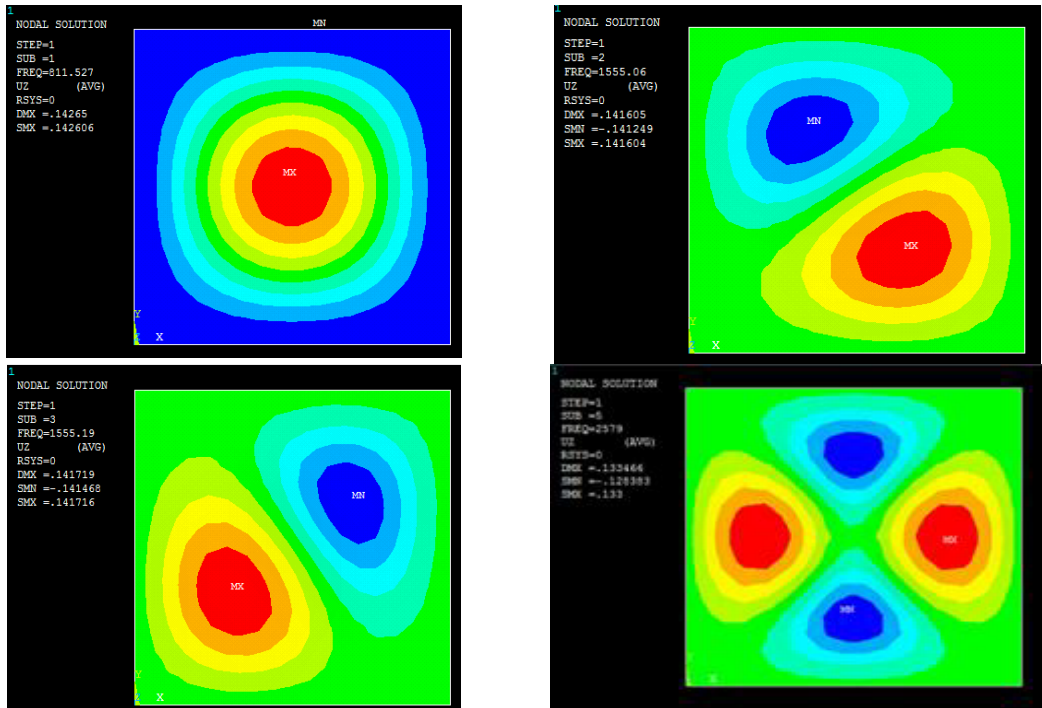


Figure 6. First four natural frequencies of functionally graded plates at volume fraction exponent $n=10$

4. Conclusion

In this study, vibration and harmonic analysis of FGM plates are analysed. Four functionally graded plates of different sets of materials are considered and their natural frequencies and frequency response amplitude at the fundamental mode are determined. Convergence tests and comparison studies have been carried out with the commercially available software (ANSYS). A four noded layered shell element (SHELL181) is used throughout the problem. The obtained results have illustrated a good agreement with those available in the literature for different volume fraction indices. It is concluded that as the volume fraction exponent increases the frequency response amplitude of FG plates increases and results also shows that for all the Functionally graded plates the frequencies decreases as the volume fraction exponent increases.

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