

Empirical Modeling of Average Cutting Speed during WEDM of Gas Turbine Alloy

Bhupinder Singh¹ and Joy Prakash Misra¹

¹Dept. of Mechanical Engineering, National Institute of Technology, Kurukshetra, India

Abstract. Cutting speed (CS) is a key performance measure to achieve optimal utilization of the WEDM process. However, input process parameters of WEDM and combination of wire and workpiece material greatly hamper CS and hence productivity and machining efficiency. Therefore, it is essential to pick the right combination of parameters and wire and workpiece material to obtain better CS. In this paper, four process parameters: T_{on} , T_{off} , S_v , and I_p were chosen to develop an empirical model for CS during WEDM of nimonic 263 to provide a guideline to the potential users of the technique. This paper describes the response surface methodology (RSM) based mathematical modeling for average cutting speed. Furthermore, analysis of variance (ANOVA) was applied to find out significant process parameters and it was depicted that pulse on time and peak current were the major parameters affecting CS. In addition, WEDMed surfaces were analysed through FE-SEM at various discharge energy levels. The WEDMed surfaces appeared in the form of micro-cracks, craters, spherical droplets and the lump of debris. It is obvious from the current investigation that input parameters have the significant influence on cutting speed. The key features of experimental procedure are also highlighted in this paper.

1 Introduction

WEDM is one of the extensively accepted non-conventional machining processes employed to manufacture components with complex shapes, profile and sharp edges that are difficult-to-machine by other traditional and non-traditional machining processes [1] and hence, this process has wide application areas including aerospace industry, medical implants, electronic industry, automobile industries, etc. It is an electro-thermal production type advanced machining process in which removal of material occurs due to melting and vaporization owing to a series of sparks between workpiece and wire electrode (thin copper, brass or tungsten of diameter 0.05-0.3 mm) submerged in a dielectric fluid (deionized water). Both electrodes are connected to a pulsed DC power supply. There is a gap between the wire and the workpiece usually ranges from 0.025 mm to 0.05 mm and is continuously maintained by a computer-controlled positioning system. The wire is kept under tension by tensioning device to overcome the inaccuracies in the machined parts. The material is removed by the series of electrical discharges between wire and workpiece in the presence of deionized water. At the point, ionization occurs and electricity flows through the ionized column of dielectric fluid between the positive and negative electrode. Once ionization takes place, the dielectric becomes heated from the flow of electricity and then changes into a gas known as plasma. Under this condition electrons rapidly pass through the ionized plasma in the form of a spark. The

positive ions from the workpiece attracted to the negatively charged electrode and the negatively charged electron collide with the workpiece and produce a spark, and this spark melts and vaporizes the small amount of material from the workpiece [2–4]. The details of the mechanism of material removal, process parameters, the influence of process parameters on measures of process performance are available in the literature [5–8]. Figure 1 illustrates the schematic of WEDM process.

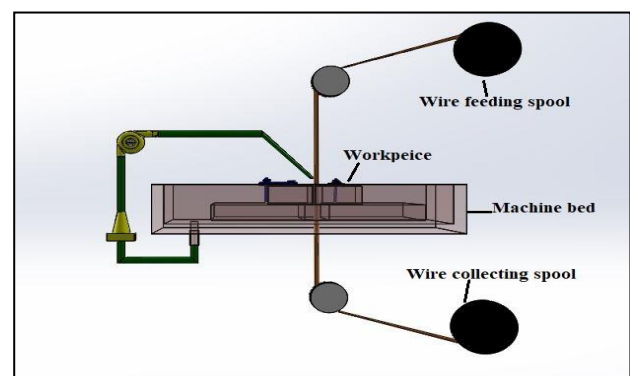


Figure 1. Schematic of WEDM process (Guitrau, 1997).

2 Experimental procedure

2.1 Experimental setup and details

The experimental investigation has been conducted on 734 sprintcut WEDM (*Make: Electronica Machine Tool*). This machine setup comprises of four major sub-components: power supply system, dielectric system, positioning system, and wire drive mechanism. The detailed functions of each sub-element are available in reference [1], [2]. From literature survey, it has been observed that most of the research work carried out on steel and steel alloys, aluminium alloys and titanium alloys [6], [9], [10]. Less research work has been reported on nickel-base super alloys and therefore it is very much essential to explore WEDM of nickel-base super alloys owing to its industrial importance in gas turbine and aerospace industry. Traditionally, combustor components have been made-out of nimonic 263 sheets. So, in this research work nimonic 263 has been selected as workpiece material. Rectangular nimonic 263 sheet of 100 mm (length), 100 mm (width), 10 mm (thickness) was used for the experimentation work and 5mm x 5mm square cuts are taken on the workpiece. Half hard-brass wire ($\phi=0.25$ mm) with 900 N/mm² is used as cutting tool, while de-ionized water was used as a dielectric. The process parameters of WEDM process are broadly classified into four groups: power supply related parameters, electrode related parameters, workpiece related parameters, and dielectric related parameters.

2.2 Design of experiments

In this study an effort has been made to find out the relationship between input and response parameters by developing empirical model for CS. This experimental study consists of four factors: T_{on} , T_{off} , S_v , I_p and each factor is having three levels. The input process parameters values and their levels for the main experiments were decided on the basis of pilot experiments. Which are conducted by using OFTA. It is obvious from the results of pilot experiments that, variation of wire feed rate, wire tension and servo feed have some insignificant effect on the CS. Therefore, these parameters were kept fixed during experimentation. The dielectric fluid temperature, conductivity, dielectric pressure and dielectric chilling medium (-2°C) were also kept constant. In this study, experimental runs are designed and planned according to the Box-Behnken design (BBD) of response surface methodology (RSM). Hence, total twenty-nine runs including five replications of centre run are required [11]. The parametric combinations for different trial runs are presented in Table 3. Table 1 and Table 2 shows the levels and values for input and fixed process parameters.

Table 1. Ranges and levels of input process parameters.

Input process parameters				
Parameters	Ranges	Levels		
		L1	L2	L3
Pulse-on time	105-131 μ s	105	118	131
Pulse-off time	30-60 μ s	30	45	60
Peak current	40-220 A	40	130	220
Servo voltage	20-80 V	20	50	80

Table 2. Values of fixed process parameters.

Fixed process parameters		
Parameters	Value	Fixing criteria
Dielectric fluid	De-ionized Water	Literature review and Pilot experiments
Peak Voltage	2 m/c unit	
Water Pressure	1 m/c unit	
Wire Feed	8 m/c unit	
Wire Tension	12 m/c unit	
Servo Feed	2200 m/c unit	
Workpiece material	Nimonic 263	Industrial application

3 Results and discussions

Table 3 shows the order, parametric combination, and design of experiments based on the coded surfaces and corresponding results for cutting speed. It is evident from Table 3 that maximum value of CS of 3.74 mm/min is obtained for experiment no. 25 (T_{on} : 118 μ s; T_{off} : 45 μ s; I_p : 130 A; and S_v : 50 V) while experiment no. 2 (T_{on} : 105 μ s; T_{off} : 60 μ s; I_p : 130 A; and S_v : 50 V) provides the lowest value of CS of 0.49 mm/min and % of change is 86.89 %. It is also evident that wire breakage has encountered in four experiments (03, 12, 19 and 22) due to wrong parametric combinations.

Table 3. Experimental design and corresponding results.

Ex. No.	Values of input process parameters				CS (mm/min)
	T_{on} (μ s)	T_{off} (μ s)	I_p (A)	S_v (V)	
01	105(-1)	30(-1)	130(0)	50(0)	1.65
02	105(-1)	60(+1)	130(0)	50(0)	0.49
03	131(+1)	30(-1)	130(0)	50(0)	WB
04	131(+1)	60(+1)	130(0)	50(0)	2.32
05	118(0)	45(0)	40(-1)	20(-1)	1.75
06	118(0)	45(0)	40(-1)	80(+1)	0.99
07	118(0)	45(0)	220(+1)	20(-1)	2.44
08	118(0)	45(0)	220(+1)	80(+1)	2.69
09	105(-1)	45(0)	40(-1)	50(0)	0.55
10	105(-1)	45(0)	220(+1)	50(0)	1.6
11	131(+1)	45(0)	40(-1)	50(0)	0.99
12	131(+1)	45(0)	220(+1)	50(0)	WB
13	118(0)	30(-1)	130(0)	20(-1)	2.15
14	118(0)	30(-1)	130(0)	80(+1)	2.12
15	118(0)	60(+1)	130(0)	20(-1)	3.03
16	118(0)	60(+1)	130(0)	80(+1)	1.04
17	105(-1)	45(0)	130(0)	20(-1)	0.91
18	105(-1)	45(0)	130(0)	80(+1)	0.74
19	131(+1)	45(0)	130(0)	20(-1)	WB
20	131(+1)	45(0)	130(0)	80(+1)	3.11
21	118(0)	30(-1)	40(-1)	50(0)	1.92
22	118(0)	30(-1)	220(+1)	50(0)	WB
23	118(0)	60(+1)	40(-1)	50(0)	0.68
24	118(0)	60(+1)	220(+1)	50(0)	2.12
25	118(0)	45(0)	130(0)	50(0)	3.74
26	118(0)	45(0)	130(0)	50(0)	3.66
27	118(0)	45(0)	130(0)	50(0)	3.69
28	118(0)	45(0)	130(0)	50(0)	3.54
29	118(0)	45(0)	130(0)	50(0)	3.64

Quadratic model is providing the lowest p value. Hence quadratic model is selected for analysis of variance for the

present study. Table 4 presents mean square, the sum of square, the degree of freedom, F value and p value for different terms of the quadratic model. The model F-value of 148.95 with corresponding p-value of <0.0001 implies that the model is highly significant as shown in Table 4. There is only a 0.01% chance that a "Model F-Value" this large could occur due to noise. Values of "Prob > F" less than 0.05 indicate model terms are significant. In this case T_{on} , T_{off} , I_p , $T_{on} \times I_p$, $T_{off} \times S_v$, $S_v \times I_p$, T_{on}^2 , T_{off}^2 , S_v^2 , I_p^2 are significant model terms. Values greater than 0.1 indicate the model terms are not significant.

Table 4. ANOVA for average cutting speed.

Source	SS	D F	MS	F-Value	P> F
Model	28.87	14	2.06	148.95	< 0.0001
A- T_{on}	4.28	1	4.28	308.91	< 0.0001
B- T_{off}	1.94	1	1.94	140.28	< 0.0001
C- S_v	0.026	1	0.026	1.88	0.2006
D- I_p	2.68	1	2.68	193.25	< 0.0001
AD	0.42	1	0.42	30.45	0.0003
BC	0.96	1	0.96	69.37	< 0.0001
CD	0.26	1	0.26	18.42	0.0016
A2	3.16	1	3.16	228.20	< 0.0001
B2	2.80	1	2.80	202.44	< 0.0001
C2	3.29	1	3.29	237.71	< 0.0001
D2	4.27	1	4.27	308.22	< 0.0001
Residual	0.14	10	0.014		
Lack of Fit	0.14	6	0.023		
Pure Error	0.000	4	0.000		
Cor Total	29.01	24			

In WEDM, cutting speed changes due to the combination of wire tool and workpiece material, the polarity of the voltage to apply, the duration of the spark, discharge energy during the spark and so on. The average cutting speed value is plotted against the process inputs to investigate the effects of input process parameters on a measure of process performance. Figure 2 illustrates the effects of T_{on} , T_{off} , I_p and S_v on CS. It is evident that T_{on} is most significant effect on CS. It is clear from the figure 2 that CS continuously increases by increasing T_{on} and decreases by decreasing T_{on} . It has been also observed that I_p is having some similar effects on CS. On the other hand, it has been observed that T_{off} and S_v is having some adverse effects on CS. Where CS values decreases by increasing the T_{off} and S_v , whereas by decreasing T_{off} and S_v some increment was noticed in CS. T_{off} plays a vital role in CS, at the lower level of T_{on} with the increase in T_{off} level CS will be lower compared with the higher level of T_{on} . Alternatively, a Smaller value of servo voltage narrows down the spark gap, which leads to more number of sparks per unit time. It speeds up the machining rate and thus the amount of material removal from the workpiece and tool [7].

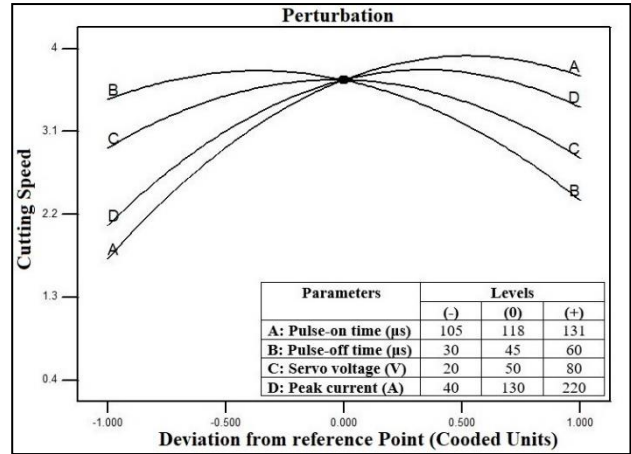
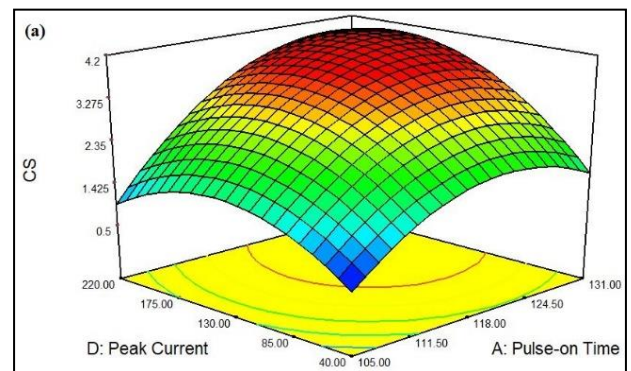


Figure 2. Effects of T_{on} , T_{off} , S_v and I_p on cutting speed [X-axis in coded value]

It is evident from analysis of variance table that the input parameters also have interaction effects on process performance characteristic. Figure 3 illustrates the interaction effects of: (a) I_p - T_{on} vs CS; (b) S_v - T_{off} vs CS; and (c) I_p - S_v vs CS. After that, a regression model of CS has been developed (in actual value) as illustrated using equation (1). The coefficient of determination (R^2) value of the developed model is found as 0.9952; is established the creditability of this model.

$$\begin{aligned}
 CS = & +3.66 + 0.99 \times A - 0.55 \times B - 0.052 \times C \\
 & + 0.64 \times D - 4.375 \times A \times B \\
 & + 0.11 \times A \times C + 0.46 \times A \times D \\
 & - 0.49 \times B \times C - 0.069 \times B \times D \\
 & + 0.25 \times C \times D - 0.95 \times A^2 \\
 & - 0.76 \times B^2 - 0.79 \times C^2 \\
 & - 0.94 \times D^2 \quad (1)
 \end{aligned}$$

(A= Pulse-on time; B= Pulse-off time; C= Peak current; D= Servo Voltage)



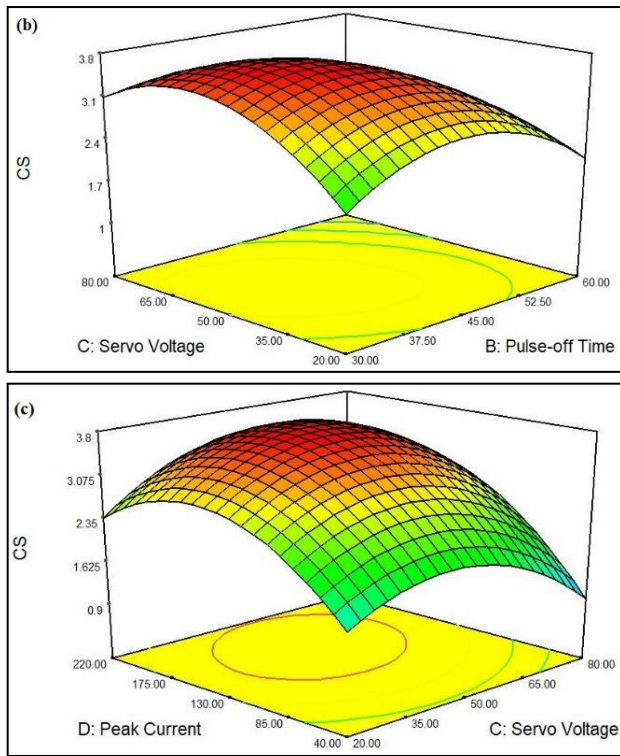


Figure 3. Interaction effects of input parameters on Cutting Speed: (a) I_p - T_{on} vs Cutting Speed; (b) S_v - T_{off} vs Cutting Speed; and (c) I_p - S_v vs Cutting Speed.

Finally, optimization is carried out using to find the optimum combination of process parameters to conduct confirmation experiments. Results of confirmation experiments are presented in table 5. Moreover, the values of CS obtained in confirmation experiments are compared with the corresponding predicted values to quantify the absolute percentage of error in prediction and thus, the prediction capability of developed model is evaluated.

Table 5. Experimental design and corresponding results.

Modified Parameters				Cutting Speed		% of Error
A	B	C	D	Predicted	Experimental	
118	37	58	138	3.75	4.22	0.11
130	32	53	144	3.90	4.52	0.13

3.1 Surface integrity analysis

Figure 4 shows the surface characteristics of the WEDMed surface of nimonic 263, obtained by using FE-SEM. Three specimens were selected for microstructure observation at low CS, average CS and higher CS. From the investigation of WEDMed surface, it is obvious that, molten metal is deposited in the form of lump of debris during WEDM. Figure 4 (a) shows the WEDMed surface at experimental condition corresponding to low discharge energy (LDE), where the parameters are set at their lowest values. Figure 4 (a) appears to be smoother as discharge craters are extremely small with the small amount of debris, fewer micro-voids are present on the surface due to LDE. Figure

4 (b) shows the surface topography at medium discharge energy (MDE), which produces the more and deep craters on the WEDMed surfaces as seen in obtained micrographs. On the other hand, at higher T_{on} and I_p , the discharge energy per duty cycle increases, which produces the wider and deeper craters, pockmarks and lump of debris on the WEDMed surfaces as seen in FE-SEM micrograph 4 (c). It is obvious from figure 4 (c) that the size of bombard is deeper and wider due to high T_{on} , which subsequently results in a high CS (3.74 mm/min) [18]. Figure 4 (d) shows the CS values for all levels: LDE, MDE and at HDE.

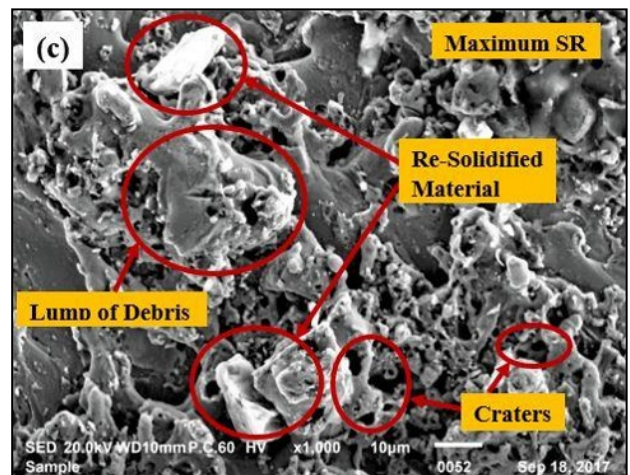
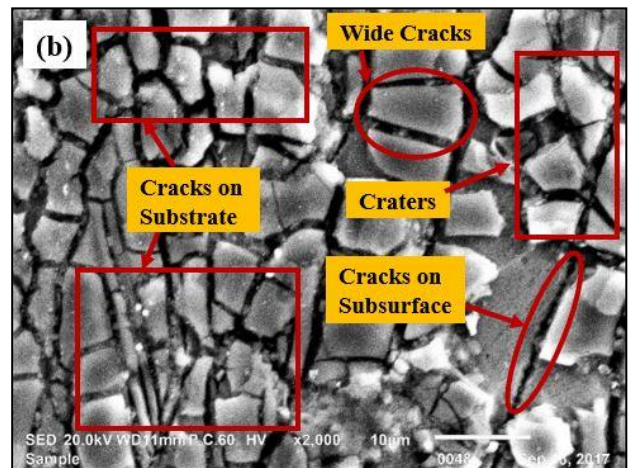
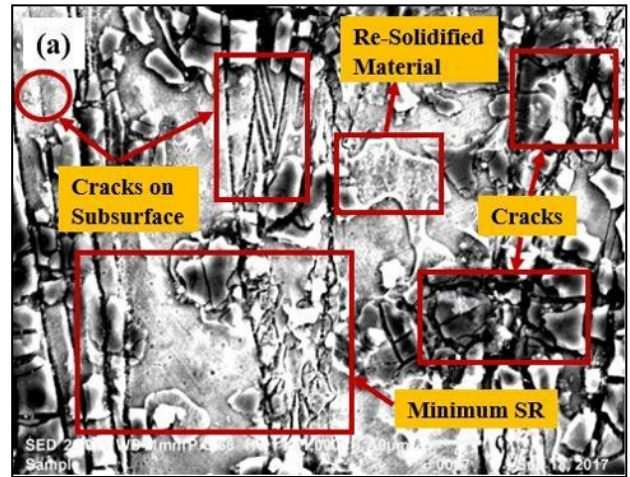


Figure 4. Microstructure of the WEDMed surfaces: (a) at low CS (Experiment no. 2); (b) at medium CS (Experiment no. 24); and (c) at high CS (Experiment no. 25).

4 Conclusions and future scope

In this study a parametric study, modeling and optimization of WEDM process of nimonic 263 has been fulfilled based on BBD were conducted to develop empirical model of process. Following conclusion has been drawn from the analysis of the results:

1. It has been observed that factor T_{on} is most significant input process parameter for CS, followed by I_p . It was also noticed that T_{off} and S_v have less significant effects on responses.
2. It is also observed that input parameters are having an interaction effect on cutting speed. It was also depicted CS increases with increase in I_p and T_{on} and with decrease in T_{off} .
3. Higher values of T_{on} and I_p leads to wire breakage. In addition, if the S_v is too low, an amount of discharge energy was absorbed by wire tool and debris in the gap cannot be flushed properly by the dielectric, it results in the arcing and wire breakages occur. Four experiments were not performed due to wrong parametric setting which results in wire breakage.
4. Surface topography reveals that WEDMed surfaces at low CS appears to be smoother as discharge craters are extremely small with the small amount of debris, fewer micro-voids are present on the surface due to low discharge energy during WEDM operation. While, Large amount of debris, craters and significant number of micro-cracks were observed on eroded surface of wire used at high CS.
5. The EDS analysis reveals, the highest percentage of migrated element is Cu: 18.22% and Zn: 6.78% is for experiment no. 25 (T_{on} : 118 μ s; T_{off} : 45 μ s; I_p : 130 A; and S_v : 50 V).
6. The developed empirical model is found best suited as it displays the very low value of prediction error (~1%) and hence, can be utilized by future users for prospective application of the technique. T_{on} : 130 μ s, T_{off} : 32 μ s, I_p : 144 A and S_v : 53 V are found optimum for the maximized value of CS.
7. Future study could consider the tribological and microstructure study of WEDM machined miniature parts: gear, spline etc. for obtaining better insight of the process.

References

1. E. Jameson, "Electrical discharge machining," (2001).
2. B. Fleming, "The EDM how-to book," p. 141, (2005).
3. K. H. Ho, S. T. Newman, S. Rahimifard, and R. D. Allen, "State of the art in wire electrical discharge machining (WEDM)," *Int. J. Mach. Tools Manuf.*, **44**, no. 12–13, pp. 1247–1259, 2004.
4. B. Singh and J. P. Misra, "A Critical Review of Wire Electric Discharge Machining," *Ann. DAAAM Proc. Int. DAAAM Symp.*, pp. 249–266, (2016).
5. N. Tosun, C. Cogun, and a. Inan, "The Effect of Cutting Parameters on Workpiece Surface Roughness in Wire EDM," *Mach. Sci. Technol.*, **7**, no. 2, pp. 209–219, (2003).
6. T. Singh, J. P. Misra, and B. Singh, "Experimental Investigation of Influence of Process Parameters on MRR during WEDM of Al6063 alloy," *Mater. Today Proc.*, **4**, no. 2, pp. 2242–2247, (2017).
7. A. Kumar, V. Kumar, and J. Kumar, "Parametric Effect on Wire Breakage Frequency and Surface Topography in WEDM of Pure Titanium," *J. Mech. Eng. Technol.*, **1**, no. 2, pp. 51–56, (2013).
8. P. Shandilya, P. K. Jain, and J. P. Misra, "Experimental investigation during wire electric discharge cutting of SiCp/6061 aluminum metal matrix composite," *Ann. DAAAM Proc. Int. DAAAM Symp.*, **21**, no. 1, pp. 1091–1092, (2010).
9. N. Tosun, C. Cogun, and G. Tosun, "A study on kerf and material removal rate in wire electrical discharge machining based on Taguchi method," *J. Mater. Process. Technol.*, **152**, no. 3, pp. 316–322, (2004).
10. R. Chalisgaonkar and J. Kumar, "Multi-response optimization and modeling of trim cut WEDM operation of commercially pure titanium (CPTi) considering multiple user's preferences," *Eng. Sci. Technol. an Int. J.*, **18**, no. 2, pp. 125–134, (2014).
11. R. H. Myers, D. C. Montgomery, and C. M. Anderson-cook, "Response Surface Methodology," Wiley, **3**, pp. 1–1247, (2009).