

# Optimization of Molding Parameters Using Taguchi Method to Increase the Electrical Conductivity and Tensile Strength of Conductive Polymer Composites

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**Abstract.** The focus of this research is to increase the electrical conductivity and tensile strength of conductive polymer composites (CPCs) materials using Taguchi method. The efforts made is by optimizing the molding parameters, using two different size of conductive fillers, ie G25 (25  $\mu\text{m}$ ) and G13 (13  $\mu\text{m}$ ) in producing CPCs material. The molding parameters used are molding time and molding temperature. S/N ratio is use to obtain the optimum molding parameters, ie the larger is better. The results showed that Taguchi method L9 (2<sup>3</sup>) succeeded in increasing the electrical conductivity and tensile strength of G25/G74/epoxy and G13/G74/epoxy composites. The highest electrical conductivity and tensile strength is on G13/G74/epoxy composites, ie 3.51 S/cm and 155.50 N/mm<sup>2</sup> respectively.

## 1. Introduction

The electrical conductivity and mechanical properties such as tensile strength are important properties to be possessed by a conductive polymer composite material. To obtain the optimum value for these both properties, it is necessary to optimize the parameters of the molding process. The parameters of the molding process used to produce the conductive polymer composites (CPCs) material are greatly affect the properties of the CPCs material produced [1-3]. Suherman et al. [1] conducted research on the effect of content, molding temperature, and molding pressure on the electrical conductivity of carbon nanotub (CNTs)/graphite/epoxy composite. The results showed that the incorporation of CNTs and graphite as a conductive materials produced a synergistic effect in improving electrical conductivity, as well as molding temperatures and molding pressure. The influence of the molding parameters of CNTs/graphite/epoxy nanocomposites to the in-plane and through-plane electrical conductivities has been observed by Suherman et al. [2]. They reported that the incorporation of CNTs and graphite materials had a positive effect in improving the electrical conductivity values of in-plane and through-plane directions, to a CNT content until 5 weight percentage (wt.%). The Taguchi method has widely used to obtain the optimum value of a molding parameter. Thanapat Sangkharat and Surangsee Dechjarern [3] conducted research on spinning process design. Ahmer et al. [4] examined the effect of time on the use of fly ash. Yizong et al. [5] analyzed the effect of molding parameters on the injection molding process using polystyrene matrix material. Sapan et al. [6] studied the benefits of benzenoacetic acid removal using CaO<sub>2</sub> nanoparticles. This research use the Taguchi method L9 (2<sup>3</sup>) to optimize the molding parameters

consisting of molding time and molding temperature using a second conductive filler with different sizes and shapes to increase the electrical conductivity and the tensile strength of the resulting conductive polymer composites.

## 2. Experimental

### 2.1 Materials

The conductive fillers used were graphite with three different sizes, ie 74  $\mu\text{m}$  (G74), 25  $\mu\text{m}$  (G25), and 13  $\mu\text{m}$  (G13). G74 which has a larger particle size, is used as the main filler, whereas G25 and G13 which has a smaller particle size are used as the second filler. The conductive fillers used as main and second fillers have different shapes, namely flakes and sphere shapes. G74 is obtained from Asbury Carbon America, while G25 and G13 are obtained from FRIway Industry, China. Epoxy resin at 6 Poise viscosity is obtained from US Composites. The description of particle size, the main and the second conductive fillers, as well as the viscosity of the epoxy resin used are obtained from the manufacturer.

### 2.2 The manufacturing of G25/G74/epoxy and G13/G74/epoxy composites

The composition based on weight percentage (wt.%) of the main, second conductive fillers and epoxy resin as the matrix are shown in Table 1. The manufacturing process of G25/G74/epoxy and G13/G74/epoxy composites is by stirring resin and hardener using a mechanical stirring machine (IKA RW 20 Digital) for 10 minutes at 25 rpm rotation. Furthermore, the main and second conductive

fillers (G25, G13 and G74) as the predefined compositions are combined with epoxy resin mixture. The G25/G74/epoxy and G13/G74/epoxy mixture are

poured into an aluminum mold. The mold is then put into the oven for 90 minutes at 150°C.

**Table 1.** Composition of G25/G74/epoxy and G13/G74/epoxy composites

CPCs material	Composition (wt.%)		
	Second fillers	Main filler	Epoxy resin
G25/G74/epoxy composites	G25 : 5, 7.5, 10	G74 : 45, 42.5, 40	50
G13/G74/epoxy composites	G13 : 5, 7.5, 10	G74 : 45, 42.5, 40	50

### 2.3 Characterization

The electrical conductivity and tensile strength of G25/G74/epoxy and G13/G74/epoxy composites material produced by different molding process parameters were measured using ASTM C 61 [7] and ASTM D3039, respectively. Scanning electron microscopy (SEM) with type S-3400 N (Hitachi) use to see the spread of main and second conductive fillers in epoxy resin.

### 2.4. Control factors and levels of molding parameters

The control factors of molding parameters are molding time ( $A_{mt}$ ), and molding temperature ( $B_{mt}$ ). Table. 2 show two control factors with three levels of molding parameters. The molding time levels ( $A_{mt}$ ) are 60, 75, and 90 min, while the levels of molding temperature ( $B_{mt}$ ) are 110, 130 and 150°C.

**Table 2.** Factors and levels of molding parameters

Symbol	Factors	Unit	Level		
			1	2	3
$A_{mt}$	Molding time	Minute	60	75	90
$B_{mt}$	Molding temperature	°C	110	130	150

## 3. Results and discussion

### 3.1 Characterization of main and second conductive fillers

Figure 1. shows the main and second conductive filler type used to produce G25/G74/epoxy and G13/G74/epoxy composites. SEM images shows that G74 as the main conductive filler has a flake shape. While G25 and G13 have flake and sphere shape.

### 3.2 The electrical conductivity of G25/G74/epoxy and G13/G74/epoxy composites

Table 3 shows the electrical conductivity generated using the molding parameters based on the Taguchi array L9 ( $2^3$ ) in generating G25/G74/epoxy and

G13/G74/epoxy composites. All parameters of the molding parameters used in this study show that G25/G74/epoxy and G13/G74/epoxy composites have different electrical conductivity. This indicates that all of the molding parameters used have an effect on the dispersion and the formation of conductive networks in the matrix polymer [8-10].

Table 3. shows that the size (25  $\mu\text{m}$  and 13  $\mu\text{m}$ ), as well as different forms (sphere and flake) of conductive fillers produce different electrical conductivity. The 9 runs performed on two different sizes and shapes of conductive fillers showed that the smaller particle size (13  $\mu\text{m}$ ) of the same shape produce the highest electrical conductivity of 2.92 S/cm (run 1). This is due to the same shape of the smaller secondary conductive filler is more effective in filling the cavity formed by the main conductive filler.

**Table 3.** Taguchi array L9 ( $2^3$ ) of molding parameters

Run	Factor and level		Electrical conductivity (S/cm)	
	A (molding time)	B (molding temperature)	13 $\mu\text{m}$	25 $\mu\text{m}$
1	60	110	2.92	1.41
2	60	130	2.26	2.72
3	60	150	2.4	2.37
4	75	110	2.57	1.49
5	75	130	1.28	1.13
6	75	150	2.78	2.07
7	90	110	2.44	1.61
8	90	130	2.74	1.58
9	90	150	2.86	1.30

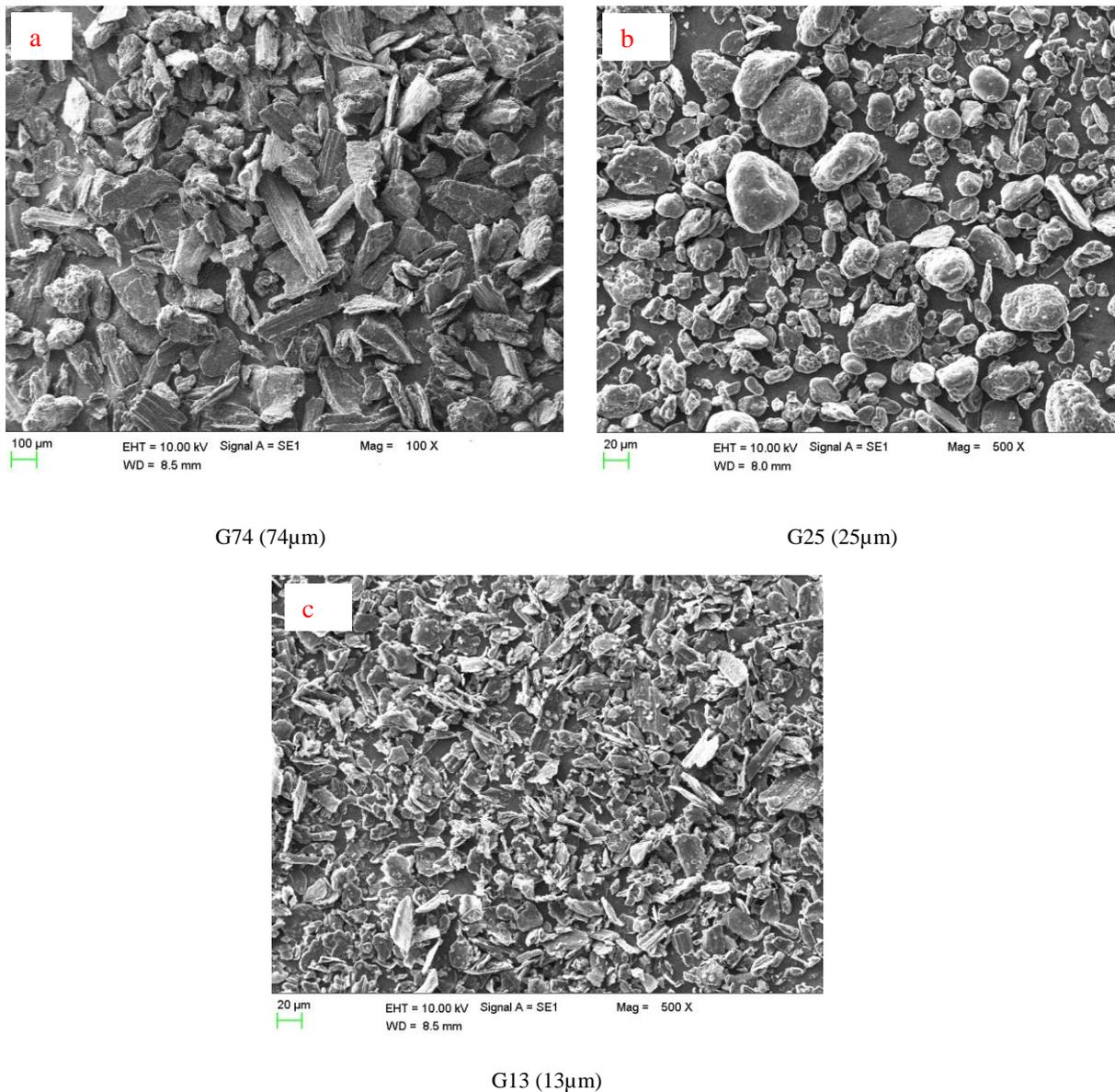


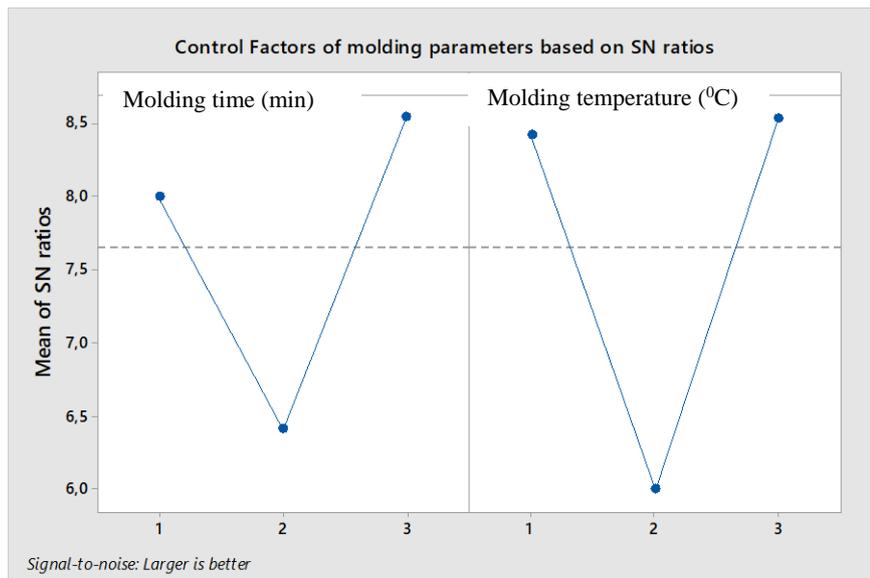
Figure 1. SEM images: (a) G74, (b) G25 and (c) G13

### 3.3 Taguchi response on molding parameters based on S/N ratio

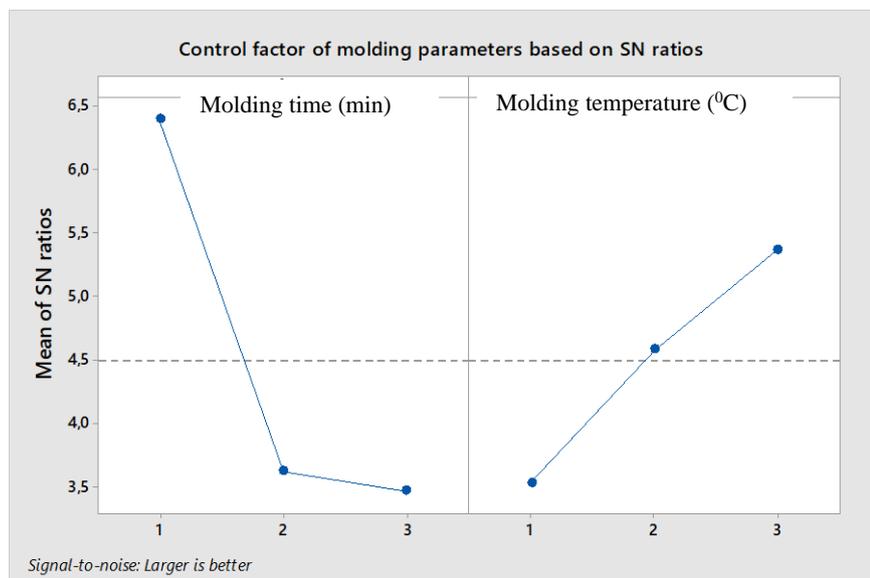
Figures 2 and 3 show the S/N ratio of the molding parameters using particle size 13 and 25µm as the second conductive filler. The optimum parameters at A<sub>3</sub> (90 minutes heating time), B<sub>3</sub> (molding temperature 150 °C) were obtained on the molding parameters of 13 µm particle size (flake shape). While in particle size 25µm (sphere shape), the optimum molding parameter obtained are A<sub>1</sub> (molding time, 60 minutes), and B<sub>3</sub> (molding temperature, 150°C). Thus, the optimum molding parameters recommended by Taguchi array L9 (2<sup>3</sup>),

(larger is better) then followed by specimens of G25/G74/epoxy and G13/G74/epoxy composites.

The Taguchi recommendations for two conductive fillers and tensile strength of different sizes and shapes are shown in Table 4. The highest electrical conductivity based on Taguchi recommendation was obtained on G13/G74/epoxy composites of 3.51 S/cm and 2.80 S/cm in G25/G74/epoxy composites. So as tensile strength, the value obtained by a smaller conductive filler (13 µm) of 155.50 N/mm<sup>2</sup> is greater when compared with a larger second filler (25 µm) of 140.42 N/mm<sup>2</sup>. The results obtained are in line with Antunes et al. [11] which states that the second conductive filler will be effective if the particle size is smaller if the conductive filler more than one.



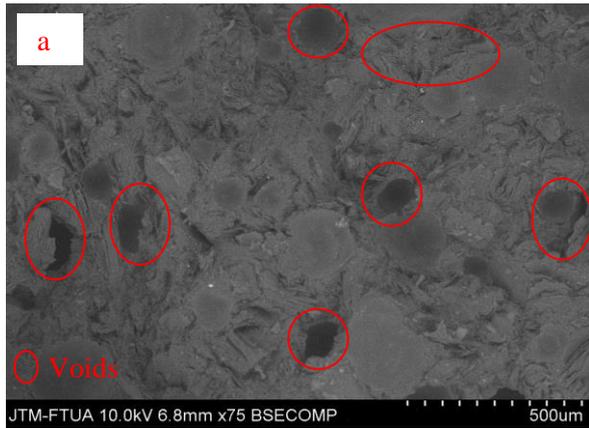
**Figure 2.** Control factors of molding parameters based on S/N ratio for particle size 13µm



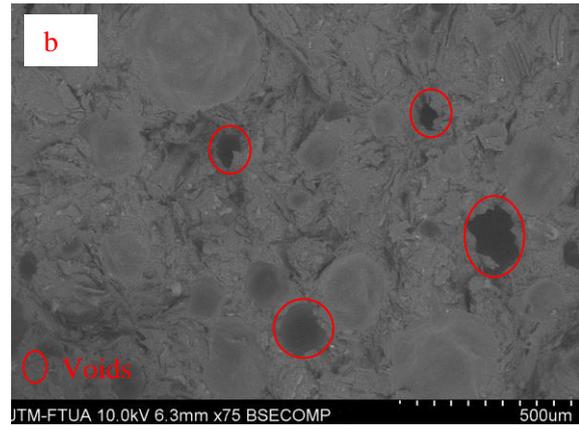
**Figure 3.** Control factor of molding parameters based on S/N ratio for particle size 25 µm

**Table 4.** Taguchi recommendation of molding parameters based on Taguchi array L9 (2<sup>3</sup>)

No	G13/G74/epoxy and G25/G74/epoxy composites	Particle size of conductive filler	Electrical conductivity (S/m)	Tensile strength (N/mm <sup>2</sup> )
1	Run 1	13 µm (flake shape)	2,92	145,50
2	Taguchi recommendation		3,51	155,50
3	Run 1	25µm (sphere shape)	1,41	127,72
4	Taguchi recommendation		2,80	140,42

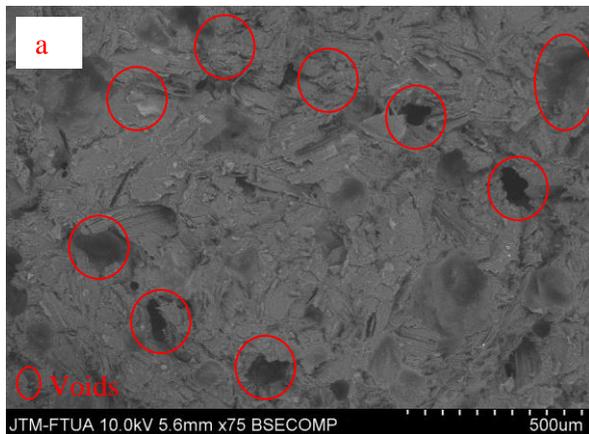


Run 1, particle size of 13 $\mu$ m

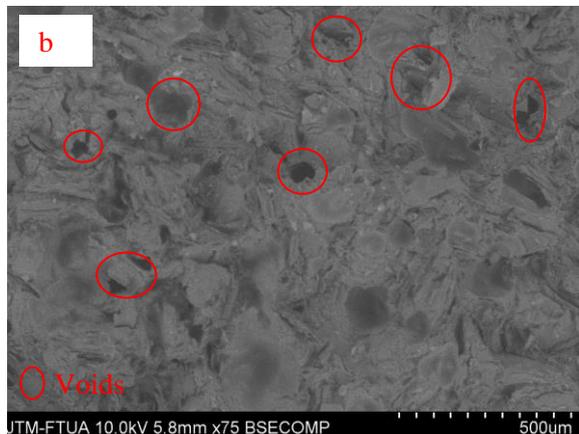


Taguchi recommendation, particle size of 13 $\mu$ m

**Figure 4.** SEM images of fracture surface of G13/G74/epoxy composites (a) Run 1, (b) Taguchi recommendation



Run 1, particle size of 25 $\mu$ m



Taguchi recommendation, particle size of 25  $\mu$ m

**Figure 5.** SEM images of fracture surface of G25/G74/epoxy composites (a) Run 1, (b) Taguchi recommendation

Figure 4. shows that run 1 of G13/G74/epoxy composite (fig.4a) has more voids compare than the G13/G74/epoxy composite (fig.4b) generated from Taguchi recommendations. Similarly, Fig. 5 shows voids formed on G25 / G74 / epoxy composite materials (fig.5a) is more than the composite materials made based on Taguchi recommendations (fig 5b). This causes the electrical conductivity and tensile strength at run 1 lower than the Taguchi recommendation [12, 13].

#### 4. Conclusion

The Taguchi method L9 ( $2^3$ ) has been used to optimize the molding parameters of G25/G74/Epoxy and G13/G74/Epoxy composites. This method successfully increases the electrical conductivity and tensile strength the composite. Both the second conductive fillers used (G25 and G13) have succeeded in increasing the electrical

conductivity and tensile strength for G25/G74/epoxy and G13/G74/epoxy composites. The G13/G74/epoxy composite increased the electrical conductivity and tensile strength from 2.92 S/cm to 3.51 S/cm (20.21%) and 145.5 N/mm<sup>2</sup> to 155.50 N/mm<sup>2</sup> (6.87%). While on G25/G74/epoxy composite, the electrical conductivity increased from 1.41 S/cm to 2.80 S/cm (98.58%) and tensile strength increased from 127.72 S/cm to 140.42 S/cm (9.94%). This condition indicates that the Taguchi method L9 ( $2^3$ ) used effectively improves the electrical conductivity and tensile strength of the resulting G13/G74/Epoxy and G25/G74/Epoxy composites.

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## References

- 1 H. Suherman, A.B. Sulong, J. Sahari. *Int. J. Mech. Mater. Eng.* **5**, 74 (2010)
- 2 H. Suherman, A.B. Sulong, J. Sahari. *Ceram. Int.* **39**, 1277 (2013)
- 3 T. Sangkharat, S. Dechjarern. *Procedia Eng.* **207**, 1713 (2017)
- 4 A.A. Siyal, K.A. Azizli, Z. Mana, H. Ullah. *Procedia Eng.* **148**, 302 (2016)
- 5 T. Yizong, Z.M. Ariff, A.M. Khalil. *Procedia Eng.* **184**, 350 (2017)
- 6 S.M. Sapana, L. Kailas, Wasewar. *J. Appl. Res. Technology* **15**, 332 (2017)
- 7 B.K. Kakati, D. Sathiyamoorthy, A. Verma. *Int. J. Hydrogen Energy* **35**, 4185 (2010)
- 8 P.C. Ma, M.Y. Liu, H. Zhang, S.Q. Wang, R. Wang, K. Wang, Y.K. Wong, B.Z. Tang, S.H. Hong, K.W. Paik, J.K. Kim. *ACS Appl. Mater. Interfaces* **1**, 1090 (2009)
- 9 N. Hu, Z. Masuda, G. Yamamoto, H. Fukunaga, T. Hashida, J. Qiu. *Composites Part A* **39**, 893 (2008)
- 10 H. Suherman, A.B. Sulong, M.Y. Zakaria, N.R. Rajendra Royan, J. Sahari. *Songklanakarinn J. Sci. Technol.* **40**, 105 (2018)
- 11 R.A. Antunes, C.L. Mara, de Oliveira, E. Gerhard, E. Volkmar. *J. Power Sources* **196**, 2945–2961 (2011)
- 12 H. Suherman, A.B. Sulong, J. Sahari. *Adv. Mater. Res.* **264-265**, 559 (2011)
- 13 N.R. Rajendran Royan, A.B. Sulong, J. Sahari, H. Suherman. *Journal of Nanomaterials* **2013** Article ID 717459 (2013)