

# Study on Stability of Round Tunnel Surrounding Rock

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**Abstract:** Tunnel excavation will lead to the immediate surrounding rock unloading caused by the surrounding rock stress release, the stability of the surrounding rock have a certain impact. In this paper, finite element software ANSYS and finite difference software FLAC3D are used to simulate the excavation and lining process of circular tunnel. The influence of excavation on the rock stability around circular tunnel is analyzed, and the effect of applying lining on the stability of surrounding rock is analyzed. Evaluation criteria selection hole displacement, stress and plastic area of three factors.

## 1 Introduction

In the case of larger buried depth and lower strength of surrounding rock, some tunneling measures should be applied to ensure the stability of the surrounding rock. The lining is to enhance the stability of the tunnel. The use of reinforced concrete and other materials in the tunnel A protective layer built around the tunnel. [1-2]

Lining construction on the one hand can enhance the stability of the tunnel and the surrounding rock mass, on the other hand can also prevent contact with the rock mass outside the tunnel to form a barrier to isolate water and air, to prevent water or air erosion, weathering ; The formation of a smooth wet weeks, so that the roughness decreases, improve the surrounding water flow, so that cross-sectional flow unit increases, reducing the unit cost of the tunnel; formation of aqueduct to reduce tunnel and surrounding rock mutual seepage; bearing Wai Rock external load, internal load and so on. It is one of the hot spots in underground engineering to study the influence of tunnel lining on the stability of surrounding rock through numerical simulation.

## 2 Project Overview

A hydropower station is a single-target project that takes power generation as its task. It is a third-stage hydropower station cascaded and developed in the basin of Podratun Zangbo. Its dam drainage area is 2453 km<sup>2</sup> with annual average flow of 132 m<sup>3</sup> / s. Spillway structures are mainly cave spillway and spillway tunnel (and diversion tunnel). The total length of the spillway tunnel is 536.66 meters, which is a circular tunnel with a diameter of 10 meters. The diversion period is made of

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cast-in-place concrete lining, with a lining thickness of 0.8 meters and faults and broken belts. The lower part of station 0 + 120 to 0 + 320 is Grade III rock, the upper part is Grade IV rock, and the fault and fracture zone are Grade V rock. [3-7]

## 3 Three - dimensional numerical model and calculation parameters selection

The section of the tunnel is circular with a diameter of 10 m and a depth of 400 m. The model range in the direction of the vertical axis is larger than 5 times the diameter of the tunnel. The Y-axis is parallel to the axis of the tunnel, the X-axis is vertical upward, and is modeled by ANSYS software. The mesh is solid element SOLID45, which is divided into 116906 units with 123,283 nodes.

The bottom of the model constrains the three-way displacement and the horizontal displacement around the constraint. The top model is established to the surface to simulate the self-weight of the upper rock mass. The rock mass is mainly composed of Group III and IV rock mass, and the fault and broken belt are Grade V rock. The lining is C40 concrete . The mechanical parameters of III, IV and V rock and concrete are shown in Table 1.

FLAC3D software calculation of bulk modulus and shear modulus parameters of the formula [8-9]:

$$\text{Bulk modulus } K = E / [3(1 - 2\mu)] \quad (1)$$

$$\text{Shear modulus } G = E / [2(1 + \mu)] \quad (2)$$

**Table 1** The mechanical parameters of the material

	type of rock	Concrete

	III	IV	V	C40
density $\rho$ (g/cm <sup>3</sup> )	2650	2450	2250	2400
Elastic Modulus E(Gpa)	8	5	1.2	32.5
Poisson's ratio $\mu$	0.25	0.3	0.4	0.2
tensile strength R (Mpa)	2.2	2	1.5	1.71
Cohesion c (Mpa)	1.1	0.5	0.2	—
Friction angle $\varphi$ (°)	47.4	35	25	—

## 4 Result analysis

### 4.1 Initial stress field

In the field of underground engineering, the existence and influence of initial geostress field can not be neglected. It is not only an important controlling factor that affects the mechanical properties of rock mass, but also one of the most important sources of deformation and destructions under the environmental conditions of rock mass. Therefore, in order to carry out engineering simulation more realistically, it is necessary to ensure the reliability of the initial geostress field. The primary purpose of initial stress field generation is to simulate the existing stress state of surrounding rock and soil before the analysis stage of interest. Figure 1 shows the initial stress field and shows that the indicator is vertical displ

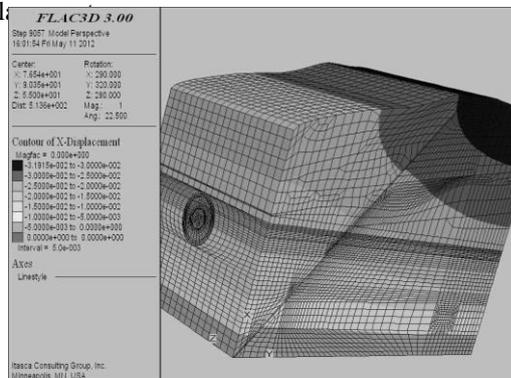


Fig.1 Initial stress field

### 4.2 Excavation and lining

After the initial geostress field is generated, excavation and lining calculation can be performed. Considering the location of faults, the analysis of displacement and stress after excavation and after applying lining mainly considers the following two planes: plane 1, the point (0, 40.62, 0) is perpendicular to the y-axis, that is, the vertical hole axis is close to the fault One side. Surface 2, the point (0,0,55) is perpendicular to the z-axis, ie the vertical plane parallel to the axis of the hole.

#### (1) Displacement and stress

Figures 2 through 9 show the vertical and maximum principal stress maps of the two selected faces after

excavation and after application of the lining. Table 2 for the corresponding data sheet.

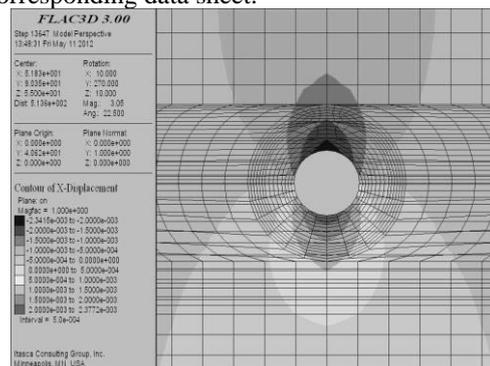


Fig.2 Vertical displacement of flat 1 after excavation

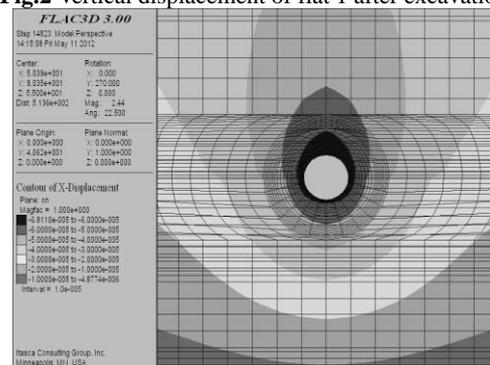


Fig.3 Vertical displacement of flat 1 after Lining

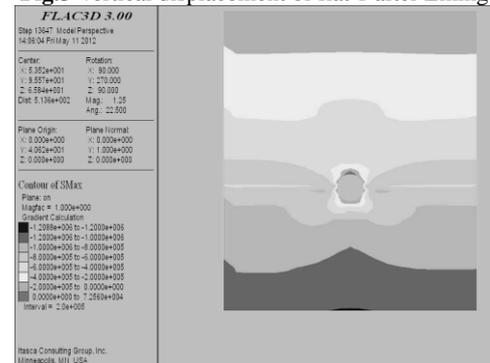


Fig.4 The main stress of flat 1 after excavation

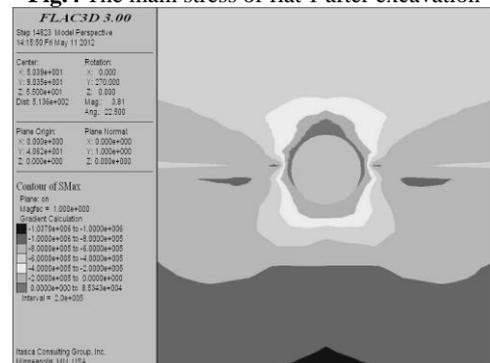
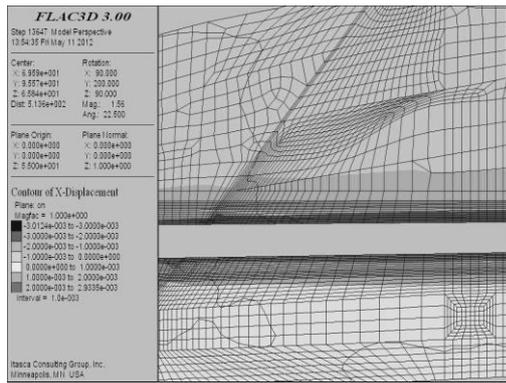
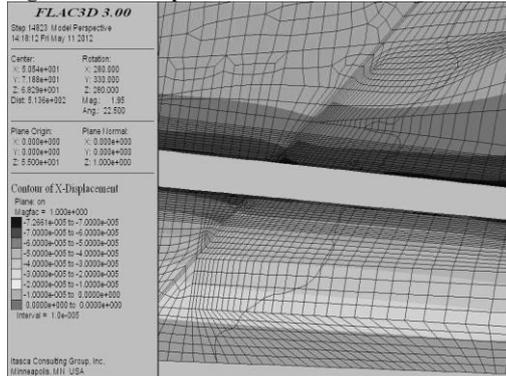


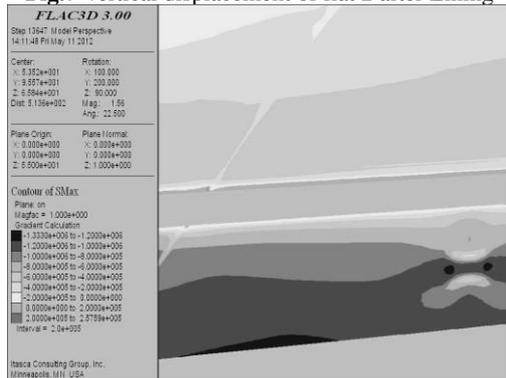
Fig.5 The main stress of flat 1 after Lining



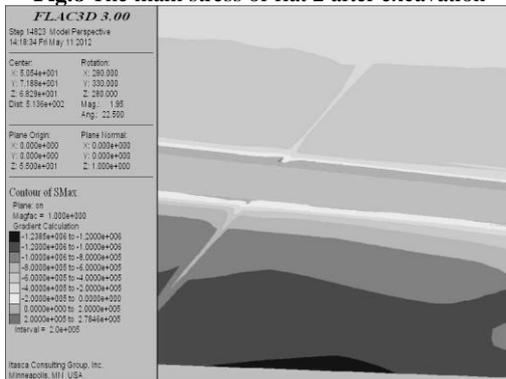
**Fig.6** Vertical displacement of flat 2 after excavation



**Fig.7** Vertical displacement of flat 2 after Lining



**Fig.8** The main stress of flat 2 after excavation



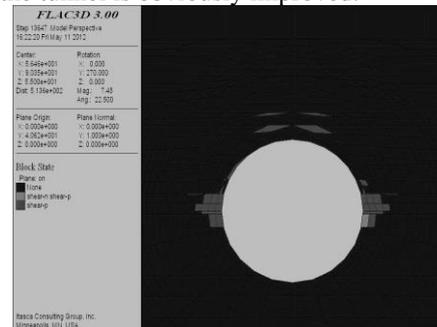
**Fig.9** The main stress of flat 2 after Lining

surface 2	Maximum displacement (m)	Cave top - $3.01 \times 10^{-3}$ Hole bottom $2.93 \times 10^{-3}$	- $7.27 \times 10^{-5}$
	The main stress (Mpa)	- 1.33	- 1.24

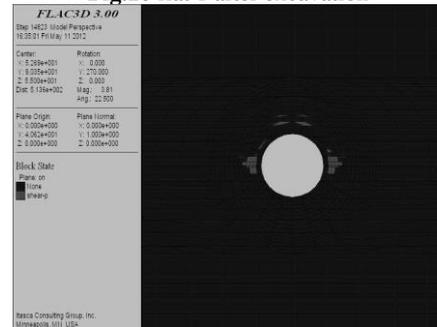
It can be seen from Table 2 that the maximum displacement at the top of the face 1 is  $-2.34 \times 10^{-3}$  m, the bottom of the hole is  $2.38 \times 10^{-3}$  m, and the maximum displacement after lining is  $-6.8 \times 10^{-5}$  m, which shows a significant improvement. The maximum principal stress after excavation is -1.21 Mpa, lining -1.04 Mpa, the stress also improved. The maximum displacement at the top of the surface 2 hole is  $-3.01 \times 10^{-3}$  m, the bottom of the hole is  $2.93 \times 10^{-3}$  m, and the maximum displacement after lining is  $-7.27 \times 10^{-5}$  m, which is obviously improved. The maximum principal stress is -1.33 Mpa after excavation and -1.24 Mpa after lining, and the stress is also improved.

(2) Plastic zone

The plastic zone is the yield zone where the pressure generated by the load around the hole exceeds the ultimate bearing capacity of the surrounding rock and causes the deformation of the local soil to be unrecoverable. Figure 10 to Figure 13 show the plastic zone of the two analyzed surfaces after excavation and after lining. It can be seen from the figure that after excavation, the plastic zone around the hole circumference and the fault is larger, but after the lining is applied, the plastic deformation caused by excavation around the tunnel is obviously improved.



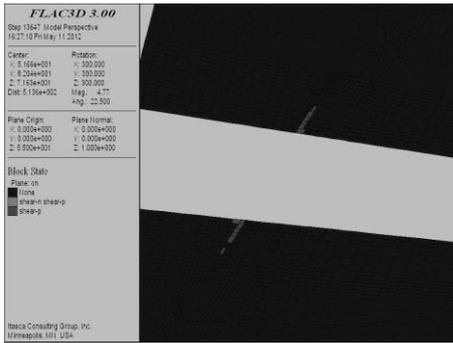
**Fig.10** flat 1 after excavation



**Fig.11** flat 1 after Lining

**Table.2** After excavation and lining the maximum displacement and the maximum principal stress

Analysis of the surface	Index	After excavation	After lining
surface 1	Maximum displacement (m)	Cave top - $2.34 \times 10^{-3}$ Hole bottom $2.38 \times 10^{-3}$	- $6.8 \times 10^{-5}$
	The main stress (Mpa)	- 1.21	- 1.04



**Fig.12** flat 2 after excavation

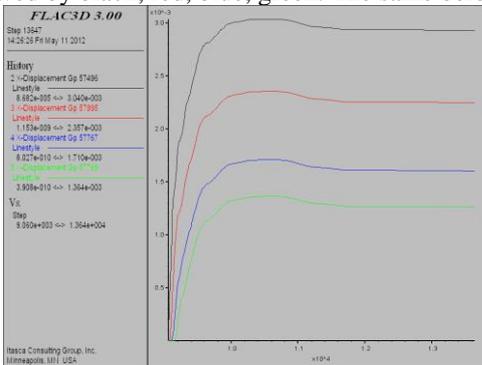


**Fig.13** flat 2 after Lining

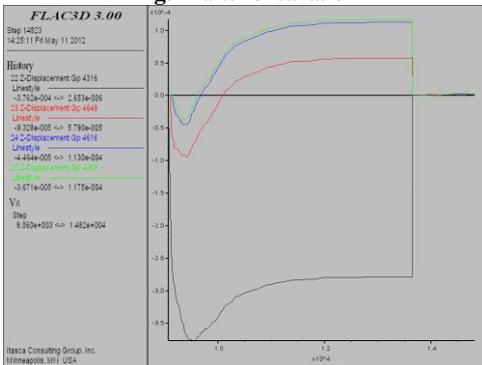
(3) Variable monitoring

The following variables were monitored during the excavation and lining calculations:

- 1) Hole bottom away from the center of 5.8 meters, 8 meters, 11 meters, 14 meters at the vertical displacement (followed by black, red, blue, green. The same below)

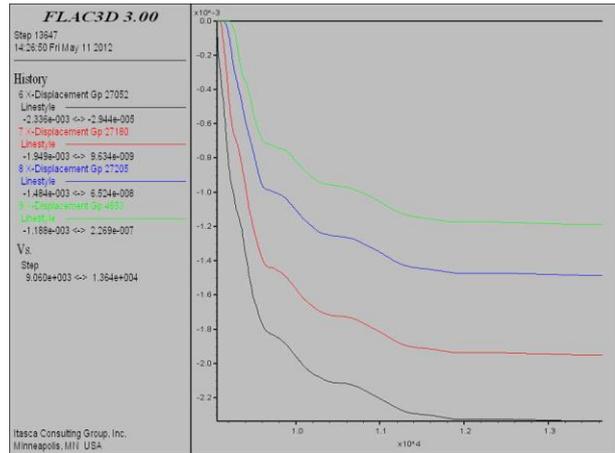


**Fig.14** after excavation

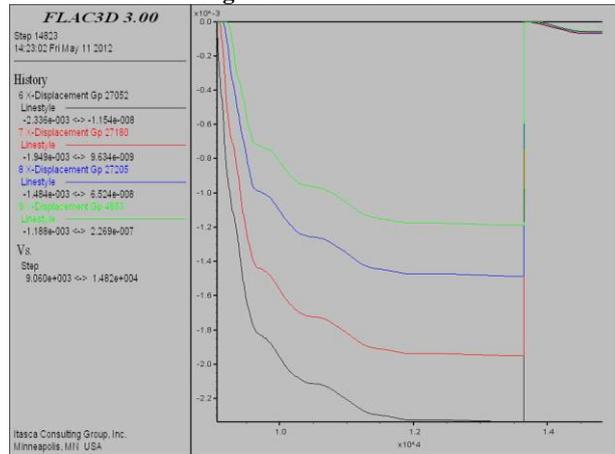


**Fig.15** after Lining

- 2) The roof from the center of the circle 5.8 meters, 8 meters, 11 meters, 14 meters at the vertical displacement

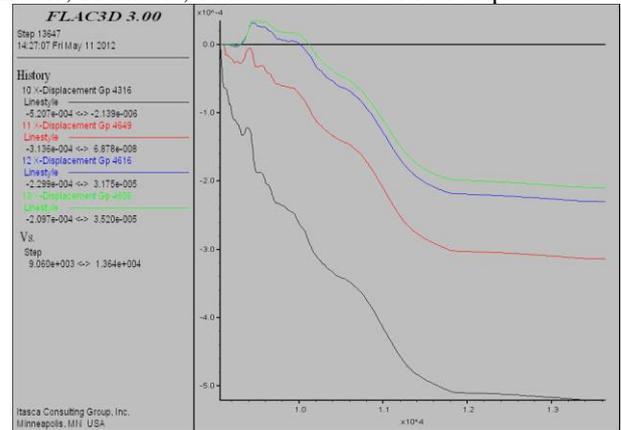


**Fig.16** after excavation

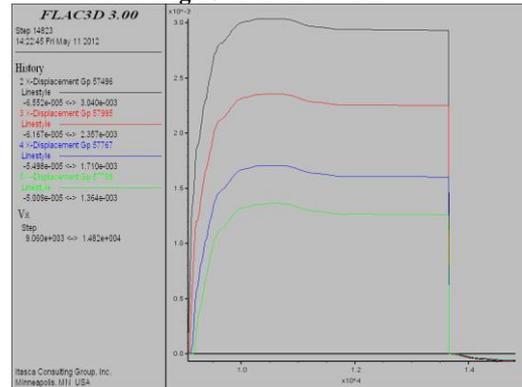


**Fig.17** after Lining

- 3) Hole on both sides from the center of 5.8 meters, 8 meters, 11 meters, 14 meters at the vertical displacement

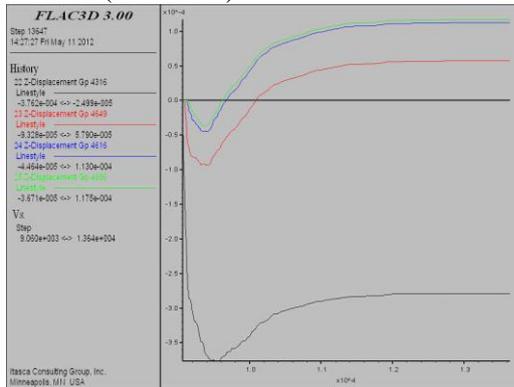


**Fig.18** after excavation

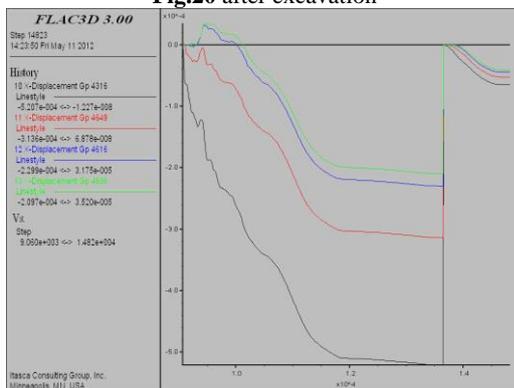


**Fig.19** after Lining

4) Hole on both sides from the center of the circle 5.8 meters, 8 meters, 11 meters, 14 meters at the horizontal displacement (z direction)



**Fig.20** after excavation



**Fig.21** after Lining

It can be seen from the figure that the closer the place to excavation, the greater the displacement, because the closer to the excavation position, the greater the stress release, the greater the impact of excavation and unloading. After the lining is applied, it can be seen from the figure that the displacements at all monitoring points are significantly reduced. Therefore, in tunnel excavation, the lining should be applied in time to ensure the stability of rock around the tunnel.

## 5 Conclusion

The numerical simulation software is used to carry out numerical excavation and lining calculation of spillway tunnel of a hydropower station. The calculation results show that the maximum displacement at the top of tunnel after excavation is  $-2.34 \times 10^{-3}$  m and the cave bottom is  $2.38 \times 10^{-3}$  m. Displacement  $-6.8 \times 10^{-5}$  m, indicating that after the lining is applied, the displacement of the perimeter of the tunnel decreases obviously and the stability of the rock around the tunnel has been improved obviously. The maximum principal stress of the perimeter of the tunnel is -1.21 Mpa and -1.04 Mpa after lining, After the excavation, the plastic zone of the surrounding rock and the surrounding rock near the fault have a larger range, and the range of the plastic zone obviously decreases after the lining is applied. The analysis shows that after the lining is applied, the displacement, stress and plastic zone of the surrounding rock of tunnel are improved, which can ensure the stability of the surrounding rock after tunnel excavation.

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