Effect of Heat Input on Porosity in High Nitrogen Steel Composite Welds

CUI Bo1,2, ZHANG Hong1,3,4a, and LIU Fengde1,4

1 College of Mechanical and Electric Engineering, Changchun University of Science and Technology, Changchun, Jilin Province, China
2 College of Automobile and Civil Engineering, Beihua University, Jilin, Jilin Province, China
3 Engineering Research Center of Laser Processing for Universities of Jilin Province, Changchun University of Science and Technology, Changchun, Jilin Province, China
4 National Base of International Science and Technology Cooperation in Optics, Changchun University of Science and Technology, Changchun, Jilin Province, China

Abstract. High-nitrogen steel plates with a thickness of 8 mm are welded with a laser-arc composite heat source for experiment to study the impact of different heat input parameters on the blowhole defect. The results show that with the increase of laser power, welding current and arc voltage, the porosity of welds decreases; with the increase of welding speed, the porosity of welds increases. Appropriately increasing the heat input helps reduce the porosity of the weld.

1 Introduction

High-nitrogen steel (HNS) has received extensive attention due to its good toughness and corrosion resistance [1-4]. With the development of smelting technology, HNS with a nitrogen content of more than 1.0% have been used in aviation, weapons, medical and cryogenic industries [5-6]. However, due to its own properties, high-nitrogen steels are prone to problems such as porosity, nitride precipitation, solidification cracks, and liquefied cracks during the welding process, which limits the wider application of high-nitrogen steels to some extent [7-9]. During the welding process, the solubility of nitrogen in the molten steel due to the nitrogen content of the high nitrogen steel is higher than the atmospheric pressure, so that the nitrogen element escapes and forms pores in the weld [10].

KAMIYA [11] conducted TIG welding experiments on high-nitrogen steels with nitrogen contents of 0.51wt% and 0.78wt%. It was found that high nitrogen steel with a nitrogen content of 0.51 wt% did not form pores during welding. For high-nitrogen steels with a nitrogen content of 0.78 wt%, there are a large number of tiny pores near the fusion line. Galloway A.M. [12] carried out argon arc welding on high nitrogen steels to study the effects of different proportions of nitrogen and helium in the shielding gas on the nitrogen content of the welds. The study found that when the nitrogen content of the protective gas accounted for 15%, the nitrogen content in the weld increased the most. Zhao Lin et al. [13] used CO2 lasers to weld high-nitrogen steels with a thickness of 3 mm. The effects of different welding heat input and different shielding gas compositions on the nitrogen content and the number of pores in the welds were studied. The results show that the higher heat input and the higher nitrogen content of the shielding gas make the tendency to produce blowholes in the weld. Miyano Y [14] used friction stir welding to weld high nitrogen steels, and studied the effect of different heat input on the microstructure and properties of welded joints. The test found that there was no porosity in the weld zone, and both the tensile strength and yield strength were higher than the base metal.

At present, there are few researches on HNS laser-arc hybrid welding, especially for the problem of pore in welding process of high-nitrogen steels [15-16]. This article focuses on the effect of heat input parameters on nitrogen content and porosity defects in welds.

2 Experimental methods

The test was performed using a side-axle hybrid welding system consisting of a 4 kW Nd:YAG laser (Model HL4006D by TRUMPF) and a power supply (Model YD-350A G2HGE by Panasonic). The test device is shown in Fig. 1.

Fig. 1 Set-up of Nd:YAG laser-GMAW hybrid welding

© The Authors, published by EDP Sciences. This is an open access article distributed under the terms of the Creative Commons Attribution License 4.0 (http://creativecommons.org/licenses/by/4.0/).
The test was carried out using a flat butt welding method. The test plate size was a high-nitrogen steel plate of 8 mm×400 mm×100 mm with a groove angle of 30°, a blunt edge of 3 mm and a butt gap of 0.4 mm. Filler wire uses an austenitic stainless steel wire with a diameter of 1.2 mm. The main chemical composition of the base metal and wire is shown in Table 1. Shielding gas is 95% Ar+5%CO2 and gas flow is 17 L/min. Welding is performed in the form of an arc in front of the laser. The laser is normally incident with an angle of 25° to the torch. The main welding process parameters tested are shown in Table 2.

Table 1. Chemical compositions of base metal and filler metal (wt%).

<table>
<thead>
<tr>
<th></th>
<th>C</th>
<th>Cr</th>
<th>Ni</th>
<th>Mn</th>
<th>Mo</th>
<th>Si</th>
<th>S</th>
<th>P</th>
<th>N</th>
</tr>
</thead>
<tbody>
<tr>
<td>Base metal</td>
<td>0.148</td>
<td>22.07</td>
<td>0.47</td>
<td>16.00</td>
<td>—</td>
<td>0.49</td>
<td>0.002</td>
<td>0.029</td>
<td>0.56</td>
</tr>
<tr>
<td>Filler wire</td>
<td>0.09</td>
<td>21.00</td>
<td>9.00</td>
<td>1.6</td>
<td>0.37</td>
<td>—</td>
<td>0.010</td>
<td>0.020</td>
<td>—</td>
</tr>
</tbody>
</table>

The X-ray detection method was used to detect the pores in the weld. N/O analyzer was used to measure the nitrogen content in the weld.

Table 2. Experimental parameters

<table>
<thead>
<tr>
<th>Welding parameters</th>
<th>Laser power $P$ [kW]</th>
<th>2.0-2.8</th>
</tr>
</thead>
<tbody>
<tr>
<td>MAG current $I$ [A]</td>
<td>230-270</td>
<td></td>
</tr>
<tr>
<td>MAG voltage $U$ [V]</td>
<td>26-30</td>
<td></td>
</tr>
<tr>
<td>Welding speed $V$ [m/min]</td>
<td>0.6-1.0</td>
<td></td>
</tr>
<tr>
<td>Defocusing amount $\Delta f$ [mm]</td>
<td>-2</td>
<td></td>
</tr>
<tr>
<td>Angle of welding torch $\theta$ [°]</td>
<td>25</td>
<td></td>
</tr>
<tr>
<td>Distance between laser and arc $D_{LA}$ [mm]</td>
<td>3</td>
<td></td>
</tr>
</tbody>
</table>

3 Results and discussion

3.1 Analysis of nitrogen behavior during welding

Fig. 2 shows the change of nitrogen content in high nitrogen steel welds during welding. It can be seen from the figure that the nitrogen in the molten pool exists as nitrogen molecules, nitrogen atoms and nitrogen ions. The solubility of nitrogen in the liquid steel is relatively large, and under the effect of 95%Ar+5%CO2 as the welding protection gas, the bath is isolated from the air and there is no nitrogen absorption process. Because nitrogen has a lower solubility in solid steel than liquid steel, excess nitrogen escapes the weld as nitrogen in the solidification process. As the solidification process progresses, the solubility of nitrogen in the steel is dynamically changing. After the molten pool is completely solidified, the concentration of nitrogen in the steel represents a balance relationship between absorbed nitrogen and escaped nitrogen, and the nitrogen sorption process is controlled by the process that absorbs nitrogen atoms and absorbs nitrogen ions faster.

![Fig. 2](image-url)

3.2 Effects of laser power on weld porosity

Fig. 3 shows X-ray inspection images of high nitrogen steel welds under different laser power conditions. It can be seen from the figure that there are pores in the weld at different laser powers, and the size and number are not the same. The number of pores is significantly less at $P=2.4$ kW, but the pore area is larger. The number of pores is the highest at $P=2.8$ kW, and the nitrogen pores are small.

![Fig. 3](image-url)

It can be seen from the figure that as the laser power increases, the porosity of the weld decreases. As the
laser power increases, the solidification time of the pool metal increases, resulting in an increase in the nitrogen evolution time. At the same time, the laser power increases, the keyhole effect becomes more intense, and the molten metal flowability increases.

3.3 Influence of arc energy on the porosity of weld

Fig. 4 and Fig. 5 are images of X-ray flaw detection of weld seam under different welding current and arc voltage. It can be obtained from the diagram that the porosity of the welding seam decreases with the increase of the welding current and the arc voltage. This is because when the arc energy is low, the effect of laser on arc compression and arc stabilization is obvious. The arc column becomes smaller, which leads to the decrease of weld width. Therefore, the area where bubbles escape from the molten pool becomes smaller. In addition, the arc energy becomes smaller, which causes the solidification time of the molten pool to become shorter. So bubbles do not have enough time to escape from the molten pool.

![Fig. 4 Welding X-ray flaw detection diagram under different welding currents](image1)

![Fig. 5 Welding X-ray flaw detection diagram under different arc voltage](image2)

3.4 Influence of welding speed on the porosity of weld

Fig. 6 shows the weld X-ray flaw detection at different welding speeds. As can be seen from the figure, the porosity of the weld increases as the welding speed increases. This is due to the fact that as the welding speed increases, the line energy per unit length of the weldment decreases and the solidification time of the weld pool shortens, so the nitrogen escape time decreases.

![Fig. 6 Welding X-ray inspection under different welding speeds](image3)

4 Conclusions

In the welding process, nitrogen absorption and nitrogen release processes occur in the molten pool. With the increase of laser power, welding current and arc voltage, the porosity of the weld decreased; as the welding speed increased, the porosity of the weld increased.

References

1. HANS B. Manufacture and application of high nitrogen steels[J]. The Iron and Steel Institute of Japan, 1996, 36(7): 909-914
3. YUJI I, RIKIO N. Effect of thermo-mechanical treatment on mechanical properties of high-nitrogen containing Cr-Mn-Ni austenitic stainless steels[J]. The Iron and Steel Institute of Japan, 1996, 36(7): 855-861


