

## Comparative study of direct and inverse problems of cracked beams

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**Abstract.** In recent decades, the analysis and evaluation of the cracked structures were hot spots in several engineering fields and has been the subject of great interest with important and comprehensive surveys covering various methodologies and applications, in order to obtain reliable and effective methods to maintain the safety and performance of structures on a proactive basis. The presence of a crack, not only causes a local variation in the structural parameters (e.g., the stiffness of a beam) at its location, but it also has a global effect which affects the overall dynamic behavior of the structure (such as the natural frequencies). For this reason, the dynamic characterization of the cracked structures can be used to detect damage from non-destructive testing. The objective of this paper is to compare the accuracy and ability of two methods to correctly predict the results for both direct problem to find natural frequencies and inverse problem to find crack's locations and depths of a cracked simply supported beam. Several cases of crack depths and crack locations are investigated. The crack is supposed to remain open. The Euler–Bernoulli beam theory is employed to model the cracked beam and the crack is represented as a rotational spring with a sectional flexibility. In the first method, the transfer matrix method is used; the cracked beam is modeled as two uniform sub-segments connected by a rotational spring located at the cracked section. In the second method which is based on the Rayleigh's method, the mode shape of the cracked beam is constructed by adding a cubic polynomial function to that of the undamaged beam. By applying the compatibility conditions at crack's location and the corresponding boundary conditions, the general forms of characteristic equations for this cracked system are obtained. The two methods are then utilized to determine the locations and depths by using any two natural frequencies of a cracked simply supported beam obtained from measurements as inputs. The two approaches are compared with a number of numerical examples for simply supported beams including one crack. The theoretical results show that the accuracy of the Rayleigh's method to predict natural frequencies decreases for higher modes when crack depth increases. It is also found that for the inverse problem, the transfer matrix method show a good agreement with those obtained from previous works done in this field.

### 1 Introduction

In the areas of civil, mechanical and aerospace engineering, the structure must fulfill some requirements such as durability, resistance, working safely and the capacity to satisfy the needs of users during its operational lifetime, which requires a continuous monitoring to detect possible damages (e.g., cracks) that allows an assessment of its state from the current structural conditions also provide a certain forecast of its future performance and information for maintenance, in order to verify its integrity and compliance with applicable regulations. The dynamic behavior of cracked beams has been studied by various analytical, numerical and experimental methods. Dimarogonas [1] and Gasch [2] presented comprehensive reviews of the dynamics of cracked structures. When a structural component is subjected to cracks, it lead to changes in structural parameters (e.g., the stiffness of a structural member such

as beam elements), which, in turn, change dynamic behavior (such as natural frequencies and mode shapes).

Damage detection of beam elements has two different aspects: the first is to study the effects of cracks on the structure parameters (mass, damping and stiffness), from a detailed numerical model based on the geometric and material properties of the structure as a direct problem. Different approaches were used to model cracks in beams, such as equivalent reduced cross-section, local bending moment and local flexibility. Ostachowicz and Krawczuk [3] gave comprehensive surveys of crack modeling approaches. Friswell and Penny [4] compare the different approaches to crack modeling, and demonstrate that for structural health monitoring using low frequency vibration, simple models of crack flexibility based on beam elements are adequate. A common approach is representing the crack by a rotational spring, but with different formulas to modeling the effect of a crack on the local flexibility [5-7].

The second can be regarded as how to detect the location and depth of the cracks, from experimentally measured data, by analyzing the changes in the vibration characteristics of the structure (natural frequencies, mode shapes, etc.), as an inverse problem. In the field of inverse problems, both analytical and numerical classes of crack detection problem were usually based on changes of natural frequencies, measuring dynamic flexibility or comparison of mode shapes [8-10]. Among the aforementioned crack identification methods, greater attention has been devoted to solve the crack problem based on changes of fundamental frequencies. Liang et al [11] developed a frequency contour plot method based on measurements of the first three natural frequencies to detect a crack in a beam. Nandwana and Maiti [12] have been extended the method to stepped beams. Lee [13] used a combination of the finite element method and the Newton–Raphson procedure to identify multiple cracks. Attar [14] used a transfer matrix method to solve a similar problem with general form of boundary conditions.

The objective of this paper is to compare the accuracy and ability of two methods to correctly predict the results for both direct and inverse problem of a simply supported beam with one crack. Several cases of crack depths and crack locations are studied. The crack is supposed to remain open. The Euler–Bernoulli beam theory is employed to model the cracked beam and the crack is represented as a rotational spring. In the first method, the transfer matrix method (TMM) is used; the cracked beam is modeled as two uniform sub-segments connected by a rotational spring located at the cracked section. The second one, based on the Rayleigh’s method (RM), the mode shapes of the cracked beam is constructed by adding a cubic polynomial function to that of the undamaged beam. By applying the compatibility conditions at crack’s location and the corresponding boundary conditions, the general forms of characteristic equations for this cracked beam system are obtained. The two methods are then utilized to determine the locations and depths by using any two natural frequencies of a cracked simply supported beam obtained from measurements as input. The two approaches are compared with a number of numerical examples for simply supported beams including one crack. The results show a good agreement with those obtained from previous works done in this fields.

## 2 Theoretical model

A simply supported cracked beam as shown in figure 1 has length  $L$  and longitudinal uniform rectangular cross section with height of  $h$ , width of  $b$  and one open traversed crack of depth  $a$  located at position  $X_1 = L_1$  from the left support of the beam. The beam is modeled as an Euler–Bernoulli in two segments joined by a rotational springs. The transverse deflection function of the beam at axial coordinate  $X$  and time  $T$ , is denoted by  $W_i(X, T)$  for two intervals of  $i = 1$  for  $0 < X < X_1$  and  $i = 2$  for  $X_1 < X < L$ .

The differential equation of motion for each segment is:

$$EI \frac{\partial^4 W_i(X, T)}{\partial X^4} + \rho A \frac{\partial^2 W_i(X, T)}{\partial T^2} = 0 ; i = 1, 2 \quad (1)$$

$E$ ;  $\rho$ ;  $A = bh$  and  $I = bh^3/12$  are Young’s modulus, density of the material, cross sectional area of the rectangular beam and moment of inertia of the uniform and homogeneous beam, respectively.

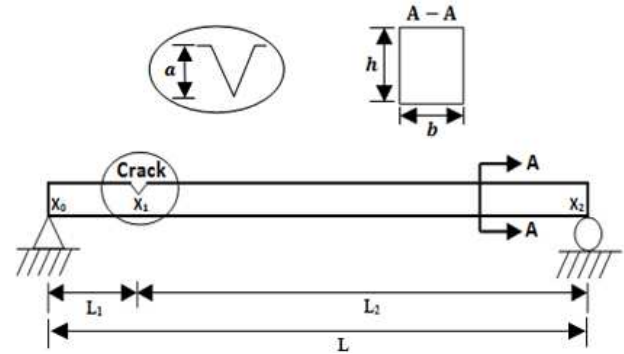


Fig.1. Model of a cracked simply supported beam.

From the above equations, the following quantities are introduced for non-dimensional analysis:

$$w_i = \frac{W_i}{L} ; t = T ; x_i = \frac{X_i}{L} ; l_i = \frac{L_i}{L} \quad (2)$$

Eq. (1) can be changed to:

$$\frac{EI}{L^4} \frac{\partial^4 w_i(x, t)}{\partial x^4} + \rho A \frac{\partial^2 w_i(x, t)}{\partial t^2} = 0 ; i = 1, 2 \quad (3)$$

The boundary conditions of this simply supported beam as non-dimensional form are:

$$x = 0 \begin{cases} \varphi_1(0) = 0 \\ M_1(0) = 0 \end{cases} ; x = 1 \begin{cases} \varphi_2(1) = 0 \\ M_2(1) = 0 \end{cases} \quad (4)$$

The continuous conditions at the crack position as non-dimensional form are:

$$x = l_1 \begin{cases} \varphi_1(l_1) = \varphi_2(l_1) \\ \theta_1(l_1) = \theta_2(l_1) - \eta M_2(l_1) \\ M_1(l_1) = M_2(l_1) \\ T_1(l_1) = T_2(l_1) \end{cases} \quad (5)$$

$\varphi$ ,  $\theta$ ,  $M$  and  $T$  are respectively the displacement, slope, bending moment and shear force expressions of the cracked beam.

Where  $\eta = \frac{Eic}{L}$ , is the non-dimensional cracked beam sectional flexibility, which is related to the ratio of crack depth to the beam height,  $\xi = a/h$ . It can be expressed as [7]:

$$\eta = \frac{h}{L} 6\pi (1 - \nu^2) f(\xi)$$

$$f(\xi) = 0.6272 \xi^2 - 1.04533 \xi^3 + 4.5948 \xi^4 - 9.9736 \xi^5 + 20.2948 \xi^6 - 33.0351 \xi^7 + 47.1063 \xi^8 - 40.7556 \xi^9 + 19.6 \xi^{10} \quad (6)$$

Where  $\nu$  is the Poisson’s ratio.

### 3 Direct problem

#### 3.1 Transfer matrix method

In order to determine natural frequencies and mode shapes, the free vibration solution can be found using the method of separation of variables as:

$$w_i(x, t) = \varphi_i(x) e^{j\omega t} \quad i = 1, 2 \quad (7)$$

Using Eq. (7) and applied to Eq. (3) yields to:

$$\varphi_i^{(4)}(x) - \beta^4 \varphi_i(x) = 0 \quad i = 1, 2 \quad (8)$$

Where:

$$\beta^4 = \frac{L^4 \rho A \omega^2}{EI} \quad (9)$$

$\omega$  is the natural frequency of the entire uniform beam. The general solution of the ordinary differential equation (9), for each segment, can be expressed as:

$$\varphi_i(x) = A_i \sin[\beta(x - x_{i-1})] + B_i \cos[\beta(x - x_{i-1})] + C_i \sinh[\beta(x - x_{i-1})] + D_i \cosh[\beta(x - x_{i-1})] \quad (10)$$

In which,  $A_i$ ,  $B_i$ ,  $C_i$ , and  $D_i$  are unknown constants associated with the  $i$ th segment ( $i = 1, 2$ ).

By substituting the boundary and continuous equations (4) and (5) into Eq. (10) for ( $i = 1, 2$ ) respectively and calculating the determinant of the matrix, the characteristic equation in this case assumes the form:

$$\eta \beta_n [\sinh(\beta_n l_1) \sinh(\beta_n l_2) \sin[\beta_n(l_1 + l_2)] - \sin(\beta_n l_1) \sin(\beta_n l_2) \sinh[\beta_n(l_1 + l_2)]] + 2 \sinh[\beta_n(l_1 + l_2)] \sin[\beta_n(l_1 + l_2)] = 0 \quad (11)$$

The above characteristic equation is solved with the help of MATLAB software using vpsolve function. Once the parameters  $\beta_n$  are obtained, the natural frequencies of the cracked beam can be obtained using the following equation:

$$\omega_{cn} = \left(\frac{\beta_n}{L}\right)^2 \sqrt{\frac{EI}{\rho A}} \quad (12)$$

Where,  $n$  is the mode range.

The constants  $A_i$ ,  $B_i$ ,  $C_i$ , and  $D_i$  can also be founded directly by the substitution method and normalizing it for the constant  $A_1$ .

#### 3.2 The Rayleigh's method

In this section, by extending the Rayleigh's method as used by Fernandez-Saez et al. [15], the fundamental frequencies and mode shapes of a simply supported beam with one crack can be obtained. The transverse deflection of the cracked beam is constructed by adding a cubic polynomial function to that of the un-cracked beam, to represent crack effects on displacement of the section of the cracked beam located to the left and the right of the crack respectively.

The general expression for the mode shapes of cracked beam is:

$$\varphi_i(X) = \sin\left(\frac{n\pi X}{L}\right) + A_i X^3 + B_i X^2 + C_i + D_i \quad 0 \leq X \leq L_i \quad (13a)$$

$$\varphi_{i+1}(X) = \sin\left(\frac{n\pi X}{L}\right) + A_{i+1} X^3 + B_{i+1} X^2 + C_{i+1} + D_{i+1} \quad L_i \leq X \leq L \quad (13b)$$

By applying the boundary conditions of this simply supported beam and the continuous conditions at the point of crack, the general expression for the mode shapes of cracked beam which is presented in non-dimensional form, can be obtained as:

$$\varphi_i(x) = \sin(n\pi x) + \eta [(n\pi)^2 \sin(n\pi l_i)] [1 - l_i] x \quad 0 \leq x \leq l_i \quad (14a)$$

$$\varphi_{i+1}(x) = \sin(n\pi x) + \eta [(n\pi)^2 \sin(n\pi l_i)] l_i [1 - x] \quad l_i \leq x \leq 1 \quad (14b)$$

The Rayleigh's method is used, so by equating the maximum values of potential energy  $U_{max}$  and kinetic energy  $T_{max}$  of the cracked simply supported beam, the natural frequencies can be obtained.

The maximum potential energy can be calculated as:

$$U_{max} = \frac{EI}{2} \left[ \int_0^{L_i} \left(\frac{M_i}{EI}\right)^2 dX + \int_{L_i}^L \left(\frac{M_{i+1}}{EI}\right)^2 dX \right] + \left[ \frac{1}{2} (\theta_{i+1} - \theta_i) M \right]_{X=L_i} = \frac{EI (n\pi)^4}{4 L^3} [1 + \eta \gamma_n] \quad (15)$$

The maximum kinetic energy can be calculated as:

$$T_{max} = \frac{\rho A \omega_{cn}^2}{2} \left[ \int_0^{L_i} (\varphi_i)^2 dX + \int_{L_i}^L (\varphi_{i+1})^2 dX \right] = \frac{\rho A \omega_{cn}^2}{2} \left[ \frac{L}{2} \left[ 1 + \eta \gamma_n \left[ 2 + \eta \left(\frac{n\pi}{3}\right)^4 l_i^2 (1 - l_i)^2 \right] \right] \right] \quad (16)$$

By equating equations (15) and (16), the  $n$ th-natural angular frequency of cracked simply supported beam is:

$$\omega_{cn} = \omega_n \left[ \frac{1 + \eta \gamma_n}{1 + \eta \gamma_n \left[ 2 + \eta \left(\frac{n\pi}{3}\right)^4 l_i^2 (1 - l_i)^2 \right]} \right]^{1/2} \quad (17)$$

Where:

$$\begin{cases} \omega_n = \left(\frac{n\pi}{L}\right)^2 \sqrt{\frac{EI}{\rho A}} \\ \gamma_n = 2 \sin^2(n\pi l_i) \end{cases} \quad (18)$$

### 4 Inverse problem

The inverse problem consists of determining the damage parameters (the location and the extent of a crack) when a certain number of measured natural frequencies are known.

The procedures for crack identification for the two methods are given below:

### 4.1 Transfer matrix method

To obtain the unknown parameters  $\eta$  and  $l_1$ , the following steps are used, which are similar to the method used in [16].

- The Eq. (11) is rewritten as:

$$\eta \beta_n [\sinh(\beta_n l_1) \sinh(\beta_n l_2) \sin[\beta_n(l_1 + l_2)] - \sin(\beta_n l_1) \sin(\beta_n l_2) \sinh[\beta_n(l_1 + l_2)]] = -2 \sinh[\beta_n(l_1 + l_2)] \sin[\beta_n(l_1 + l_2)] \quad (19)$$

- Calculating  $\beta_1$  and  $\beta_2$  from Eq. (9) by utilizing the two measured frequencies  $\omega_{c1}$  and  $\omega_{c2}$  ;

- Substituting  $\beta_1$  and  $\beta_2$  separately into Eq. (19) and dividing these two equations, the non-dimensional crack section flexibility  $\eta$  can then be cancelled out and the following identification equation can be obtained:

$$\frac{\beta_1 [\sinh(\beta_1 l_1) \sinh(\beta_1 l_2) \sin(\beta_1) - \sin(\beta_1 l_1) \sin(\beta_1 l_2) \sinh(\beta_1)]}{\beta_2 [\sinh(\beta_2 l_1) \sinh(\beta_2 l_2) \sin(\beta_2) - \sin(\beta_2 l_1) \sin(\beta_2 l_2) \sinh(\beta_2)]} = \frac{\sinh(\beta_1) \sin(\beta_1)}{\sinh(\beta_2) \sin(\beta_2)} \quad (20)$$

- The position of the crack  $l_1$ , can be determinate with the help of MATLAB software using solve function;

- After obtaining  $l_1$ , the non-dimensional crack sectional flexibility  $\eta$  can be determined from Eq. (11), and the crack depth  $a$  can then be obtained from Eq. (6).

### 4.2 The Rayleigh's method

In this section, the inverse problem can be solved by using Eq. (14) in Ref. [17], as:

$$\frac{\Delta \omega_n}{\omega_n} = \frac{\eta \gamma_n}{2} \quad (21)$$

Where:

$$\Delta \omega_n = \omega_n - \omega_{cn} \quad (22)$$

- Calculating  $\omega_1$  and  $\omega_2$  from Eq. (18) and by utilizing the two measured frequencies  $\omega_{c1}$  and  $\omega_{c2}$ ,  $\Delta \omega_1$  and  $\Delta \omega_2$  can be obtained;

- Substituting  $\frac{\Delta \omega_1}{\omega_1}$  and  $\frac{\Delta \omega_2}{\omega_2}$  separately into Eq. (21) and dividing these two equations, the non-dimensional crack section flexibility  $\eta$  can then be cancelled out and the following identification equation can be obtained:

$$\frac{\Delta \omega_1}{\omega_1} \frac{\omega_2}{\Delta \omega_2} = \frac{\gamma_1}{\gamma_2} \quad (23)$$

- The position of the crack  $l_1$ , can be determinate with the help of MATLAB software using solve function;

- After obtaining  $l_1$ , the non-dimensional crack sectional flexibility  $\eta$  can be determined from Eq. (11) and the crack depth  $a$  can then be obtained from Eq. (6).

## 5 Results and discussion

In order to validate the study presented in this paper and to show the effectiveness and also the limitations of the two methods, results obtained by applying these two

methods are compared with the available data for single open cracked simply supported beam.

The material parameters for an undamaged simply supported beam are:  $E = 2.1 \times 10^{11} Pa$ ,  $\nu = 0.3$ ,  $\rho = 7860 kg/m^3$ , and its dimensions are:  $L = 0.5 m$ ,  $h = 0.02 m$ ,  $b = 0.012 m$ .

Table 1 shows comparison of the first three natural frequencies of undamaged beam obtained from the two methods with what computed by [18]. The results show that both methods yield the same exact frequencies and agree well with those obtained from [18].

**Table 1.** Comparison of frequencies of undamaged beam, obtained by two methods and results given by Ref. [18].

	$\omega_1$	$\omega_2$	$\omega_3$
[18]	1178.160	4712.577	10603.252
1st method	1178.141	4712.566	10603.274
2nd method	1178.141	4712.566	10603.274

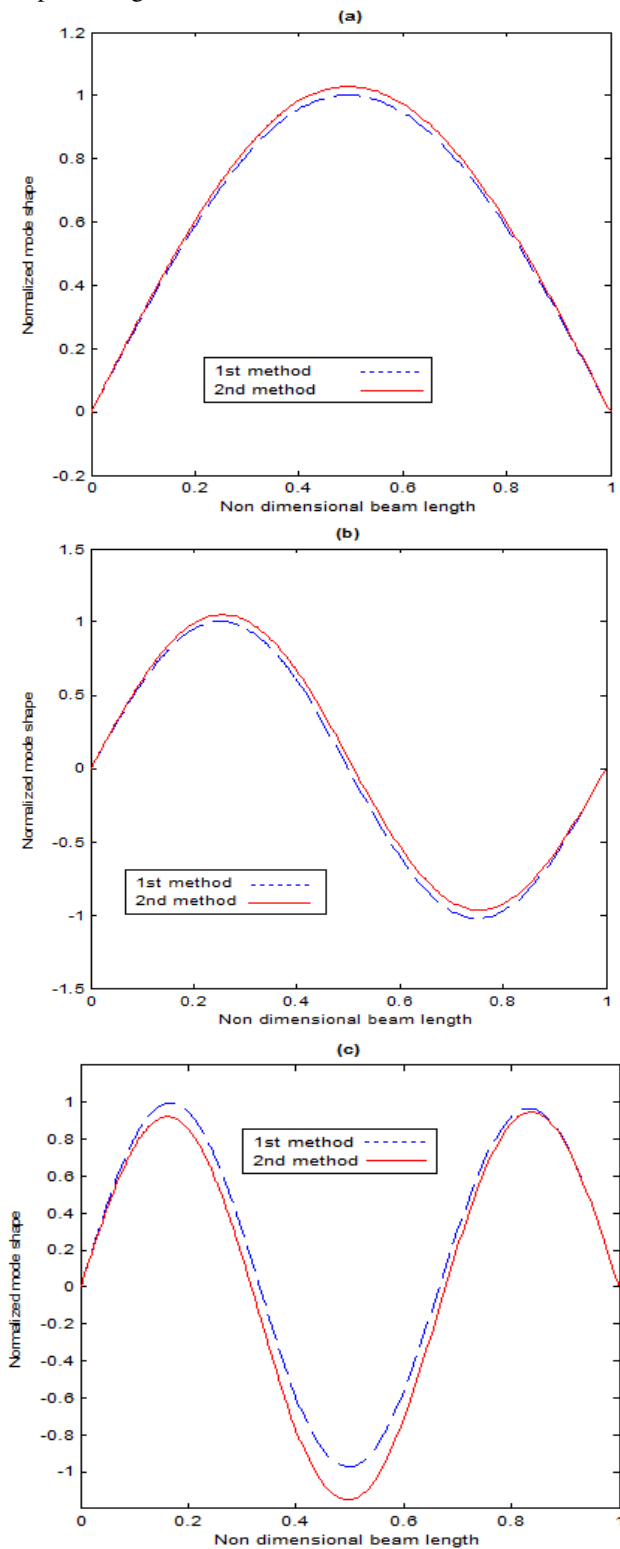
### 5.1 Direct problem

The lowest three natural frequencies of transverse vibration are calculated by the two methods, and compared with what reported by [19] for the damaged beam with one crack. The results for various crack locations and depths, given in Table 2, show a reasonable agreement between the two methods results and those achieved by [19] for all cases of the cracked beam, but the difference between natural frequencies increases for higher order modes.

**Table 2.** Comparison of first three natural frequencies of cracked beams, obtained by two methods and results given by Ref. [19] for various crack location and depth.

Case number	$l_1$	$\xi$	Methods	Natural frequencies, $\omega_{cn}$ (rad/s)		
				$\omega_{c1}$	$\omega_{c2}$	$\omega_{c3}$
1	0.1	0.1	[19]	1177.660	4705.604	10573.663
			TMM	1177.709	4706.310	10576.662
			RM	1177.709	4706.234	10574.665
2	0.2	0.3	[19]	1162.672	4557.815	10281.642
			TMM	1164.032	4570.851	10306.810
			RM	1164.036	4518.740	9675.567
3	0.3	0.2	[19]	1165.559	4644.925	10587.306
			TMM	1166.720	4651.012	10588.734
			RM	1166.721	4631.081	10562.019
4	0.3	0.3	[19]	1149.363	4563.174	10568.267
			TMM	1151.851	4575.368	10571.089
			RM	1151.858	4477.435	10428.520
5	0.4	0.2	[19]	1160.876	4686.538	10544.768
			TMM	1162.459	4688.896	10550.062
			RM	1162.460	4677.927	10429.644
6	0.4	0.4	[19]	1105.78	4608.053	10369.596
			TMM	1110.837	4614.974	10384.937
			RM	1110.847	4416.368	8607.153
7	0.5	0.2	[19]	1159.108	4712.566	10436.419
			TMM	1160.849	4712.566	10451.318
			RM	1160.849	4712.566	10105.454
8	0.5	0.4	[19]	1099.580	4712.566	9964.053
			TMM	1104.527	4712.566	10003.928
			RM	1104.528	4712.566	6723.939

Figure 2 represents plots of the corresponding mode shapes, using the two methods.



**Fig.2.** Comparison of the two methods for first three mode shapes of beam having one crack.  $l_1=0.4$  ;  $\xi=0.2$ . (a) 1<sup>st</sup> mode shape, (b) 2<sup>nd</sup> mode shape and (c) 3<sup>rd</sup> mode shape.

Table 3 shows comparison of the first three relative errors of natural frequencies (R.E.N.F) obtained by the two methods for various crack location and depth, where:

$$\text{R. E. N. F (\%)} = \left| \frac{\omega_{cn1} - \omega_{cn2}}{\omega_{cn1}} \right| \times 100 \quad (24)$$

$\omega_{cn1}$  and  $\omega_{cn2}$  are the nth calculated natural frequencies by the first and the second methods respectively.

As can be seen, the two methods can approximate first natural frequencies of cracked beam with high accuracy for various crack locations and depths. Also the two methods can approximate second natural frequencies of cracked beam with maximum error less than 5% in the 6th case when the crack location/ depth are respectively (0.4, 0.4), but the difference between natural frequencies increases for the third mode of vibration.

**Table 3.** Comparison of relative error between first three natural frequencies, obtained by the two methods for various crack location and depth.

Case number	1st R.E.N.F (%)	2nd R.E.N.F (%)	3rd R.E.N.F (%)
1	≈ 0	0.001	0.018
2	≈ 0	1.140	6.124
3	≈ 0	0.428	0.252
4	≈ 0	2.140	1.348
5	≈ 0	0.233	1.141
6	≈ 0	4.303	17.118
7	≈ 0	≈ 0	3.309
8	≈ 0	≈ 0	32.787

## 5.2 Inverse problem

The inverse problem is solved by using the exact first three frequencies used in [19] as inputs from various cases.

**Table 4.a.** Comparison of predicted and actual crack parameters for various crack location and depth by using  $\omega_{c1} - \omega_{c2}$ .

Case	Methods	$\omega_{c1} - \omega_{c2}$			
		$l_1^*$	Error (%)	$\xi^*$	Error (%)
1	Method1	0.1002	0.2473	0.1054	5.4543
	Method2	0.1005	0.5028	0.1500	50.0562
2	Method1	0.2000	0.0041	0.3128	4.2935
	Method2	0.2097	4.8554	0.4007	33.5849
3	Method1	0.2999	0.0004	0.2099	4.9612
	Method2	0.3031	1.0639	0.2871	43.5758
4	Method1	0.2999	0.0005	0.3128	4.2947
	Method2	0.3070	2.3661	0.4056	35.2128
5	Method1	0.4000	0.0002	0.2099	4.9622
	Method2	0.4006	0.1726	0.2880	44.0040
6	Method1	0.3999	0.0001	0.4126	3.1733
	Method2	0.4028	0.7158	0.5087	27.1855
7	Method1	0.5003	0.0652	0.2099	4.9610
	Method2	0.5	0	0.2878	43.9407
8	Method1	0.4998	0.0322	0.4115	2.8772
	Method2	0.5	0	0.5073	26.8415

Tables 4a-4c show the comparison of predicted ( $l_1^*$ ,  $\xi^*$ ) and actual ( $l_1$ ,  $\xi$ ) crack parameters using any two of these three frequencies.

In the majority of cases, the two methods cannot provide a unique value for the non-dimensional crack position  $l_1^*$ , which require usually an initial guess closest to the solution. This is due to the symmetric of crack locations

(i.e., 0.2 and 0.8) when the boundary conditions are also symmetric (i.e., simply supported).

**Table 4.b.** Comparison of predicted and actual crack parameters for various crack location and depth by using  $\omega_{c1} - \omega_{c3}$ .

Case	Methods	$\omega_{c1} - \omega_{c3}$			
		$l_1^*$	Error (%)	$\xi^*$	Error (%)
1	Method1	0.1000	0.0881	0.1056	5.6217
	Method2	0.1005	0.5714	0.1499	49.9553
2	Method1	0.2000	0.0012	0.3128	4.2958
	Method2	0.2081	4.0728	0.4027	34.2600
3	Method1	0.2999	≈ 0	0.2099	4.9609
	Method2	0.3005	0.1801	0.2887	44.3610
4	Method1	0.2999	0.0001	0.3128	4.2944
	Method2	0.3012	0.4000	0.4097	36.5950
5	Method1	0.3999	0.0002	0.2099	4.9624
	Method2	0.3994	0.1495	0.2883	44.1763
6	Method1	0.4000	≈ 0	0.4126	3.1732
	Method2	0.3974	0.6369	0.5105	27.6268
7	Method1	0.2467	50.6406	0.2941	47.0685
	Method2	0.4817	3.6403	0.2883	44.1548
8	Method1	0.2362	52.7556	0.5375	34.3815
	Method2	0.4646	7.0734	0.5093	27.3352

It is observed that the crack identification results for normalized crack location are relatively acceptable. The errors in the 7<sup>th</sup> and 8<sup>th</sup> cases are generally the highest for the 1<sup>st</sup> method.

It is obvious that the crack identification results for normalized crack depth are not satisfactory; this is due to the deferred behavior of the flexibility coefficient.

**Table 4.c.** Comparison of predicted and actual crack parameters for various crack location and depth by using  $\omega_{c2} - \omega_{c3}$ .

Case	Methods	$\omega_{c2} - \omega_{c3}$			
		$l_1^*$	Error (%)	$\xi^*$	Error (%)
1	Method1	0.1002	0.2473	0.1054	5.4543
	Method2	0.1005	0.5028	0.1500	50.0562
2	Method1	0.2000	0.0041	0.3128	4.2935
	Method2	0.2097	4.8554	0.4007	33.5849
3	Method1	0.2999	0.0004	0.2099	4.9612
	Method2	0.3031	1.0639	0.2871	43.5758
4	Method1	0.2999	0.0005	0.3128	4.2947
	Method2	0.3070	2.3661	0.4056	35.2128
5	Method1	0.4000	0.0002	0.2099	4.9622
	Method2	0.4006	0.1726	0.2880	44.0040
6	Method1	0.3999	0.0001	0.4126	3.1733
	Method2	0.4028	0.7158	0.5087	27.1855
7	Method1	0.5003	0.0652	0.2099	4.9610
	Method2	0.5	0	0.2878	43.9407
8	Method1	0.4998	0.0322	0.4115	2.8772
	Method2	0.5	0	0.5073	26.8415

## 6 Conclusion

Two methods used to solve the direct and inverse problems of a simply supported beam with one crack are

compared in this paper. The Euler–Bernoulli beam theory is employed to model the cracked beam and the crack is represented as a rotational spring. This study allows making the following conclusions:

- The frequencies decreased when the crack is deeper;
- The crack depth has no effects on the second natural frequencies at the mid-span;
- The natural frequencies predicted by the two methods agree well with those obtained from previous work but the error increases for higher modes of vibration;
- The crack parameters predicted in the numerical examples show that both methods are theoretically capable of estimating the location of cracks and with less performance the crack depths.

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