Increasing of the carbide cutting tool life by developing the multilayer coatings

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Abstract. The paper presents the results of studying the structural parameters and mechanical properties of multi-element coatings based on TiZrN, TiZrAlN, TiZrCrN, and TiNbAlN. The phase composition, the structural parameters, and the mechanical properties of such coatings are shown to depend on the design of cathode evaporators and the machine layout at the moment of application. Compared to TiN coating, multi-element coatings have higher residual compressive stress, smaller CSR, higher microdeformations of the crystal lattice, better mechanical properties, yet weaker adhesion to the tool base. Based on studying their structural parameters and mechanical properties, we have designed double-layer coatings. Use of such multi-layer coatings prolongs the tool life of carbide plates compared to TiN coating.

1 Introduction

Multi-layer coatings are increasingly used to improve the efficiency of cutters [1-4]. The efficiency of such coatings depends on the mechanical properties of individual layers with specific functions [5, 6]. The mechanical properties of coatings depend on their deposition. Changing the layout of the machine and the design of cathodes has a significant impact on the mechanical properties of coatings [7-13]. Therefore, by changing the deposition conditions, we can adjust the properties of multi-layer coatings.

This research is to improve the efficiency of carbide tools by adjusting the layer-specific composition of multi-layer coatings.

2 Methodology of Experiment

Durable coatings were applied to MK8 carbide plates using a Bulat-6 machine. The chemical composition of such coatings was identified by quantitative X-ray analysis on a MAP-4 machine with ZAF adjustments being factored in. The parameters of the coating structure (lattice spacing \(a\), half-width of the X-ray diffractive line \(\beta_{111}\)) and the residual compressive stresses \(\sigma_0\) were studied by means of a ДРОН-3М diffractometer; relative microdeformations of the crystal lattice \(\Delta a/a\) and the coherent scattering regions (CSR) \(D\) were calculated as in [14]. Microhardness \(H_v\), first-kind elasticity modulus \(E\), fracture toughness \(K_{IC}\) were determined as in [15]. The adhesion strength was evaluated on the bases of the stratification coefficient calculated using a TK-2M hardness tester as in [1]. The efficiency of MK8 carbide plates was evaluated based on the tool life when turning workpieces made of 38XГН steel.

3 Methodology of Experiment

The multi-layer coating architecture has been selected based on their application in continuous turning as recommended in [2, 6, 16]. According to those papers, the upper layer should create favorable interaction of machined and tool materials at the front surface of the cutter to lower equivalent stresses and stabilize the shape of the cutting wedge. At the same time, in order to contain the fracturing processes, it is desirable that this layer has high mechanical properties as well as high level of its own residual compressive stress that contribute to the generation of higher normal compressive stresses during the cutting. As shown in [2, 4], multi-element coatings, i.e. three-element coatings based on modified titanium nitride, are the best when it comes to meeting such requirements. Beside the above requirements, coatings should have strong adhesion to the tool base; single-element coatings are adhesion-stronger than their multi-element counterparts [1, 2].

Based on the above, we studied TiN, TiZrN, TiZrAlN, TiZrCrN and TiNbAlN which were then used as layers in multi-layer coatings. TiZrN coatings were applied by two cathodes of titanium and zirconium located opposite to each other; TiZrAlN was applied by the same cathodes plus a cathode made of a titan-aluminum alloy. TiZrCrN was applied by composite cathodes: two titanium cathodes with zirconium inserts and one titanium cathode with a chromium insert. Table 1 presents the chemical composition of the coatings.

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Table 1. Chemical composition of coatings.

<table>
<thead>
<tr>
<th>Coating</th>
<th>Ti</th>
<th>Zr</th>
<th>Cr</th>
<th>Nb</th>
<th>Al</th>
</tr>
</thead>
<tbody>
<tr>
<td>TiZrN</td>
<td>57.2</td>
<td>42.8</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>TiZrAlN</td>
<td>57.5</td>
<td>39.75</td>
<td></td>
<td></td>
<td>2.8</td>
</tr>
<tr>
<td>TiNbAlN</td>
<td>83.4</td>
<td></td>
<td></td>
<td>14.5</td>
<td>2.1</td>
</tr>
<tr>
<td>TiZrCrN</td>
<td>75.4</td>
<td>13.4</td>
<td>11.2</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

TiZrN and TiZrAlN are biphasic coatings. TiZrN diffraction pattern is shown in Figure 1a. As shown there, there are two diffraction peaks that are identified as TiN (111) and ZrN (111), both having a cubic crystal lattice. At an angle of 2θ=35.2 grad. between them, there is a diffraction peak identifiable as solid TiZrN solution (111). According [6, 15], such coatings have a multi-layer structure where the multi-layers of separate phases and the solid solution alternate to improve the mechanical properties. TiNbAlN and TiZrCrN are uniphasic coatings. The diffraction patterns of these coatings (see Figure 1b) only show one high-intensity diffraction peak identifiable as TiN (111). Being uniphasic proves the homogeneity of such coatings and lack of multi-layer structure.

Table 2 presents the results of studying the structural parameters of multi-element coatings compared to TiN.

Table 2. Structural parameters and mechanical properties.

<table>
<thead>
<tr>
<th>Coating</th>
<th>TiN</th>
<th>TiZrN</th>
<th>TiZrAlN</th>
<th>TiNbAlN</th>
<th>TiZrCrN</th>
</tr>
</thead>
<tbody>
<tr>
<td>а, nm</td>
<td>0.4335</td>
<td>0.4356</td>
<td>0.4344</td>
<td>0.4309</td>
<td>0.4279</td>
</tr>
<tr>
<td>β_{111}, deg</td>
<td>0.40</td>
<td>0.82</td>
<td>1.06</td>
<td>0.70</td>
<td>0.59</td>
</tr>
<tr>
<td>σ₀, MPa</td>
<td>-775</td>
<td>-1352</td>
<td>-1487</td>
<td>-1875</td>
<td>-1422</td>
</tr>
<tr>
<td>D, nm</td>
<td>26.0</td>
<td>11.63</td>
<td>8.90</td>
<td>13.70</td>
<td>16.56</td>
</tr>
<tr>
<td>Δа/а 10^{-3}</td>
<td>4.8</td>
<td>10.6</td>
<td>13.8</td>
<td>9.1</td>
<td>7.5</td>
</tr>
<tr>
<td>H, GPa</td>
<td>24.2</td>
<td>36.0</td>
<td>39.8</td>
<td>37.6</td>
<td>36.8</td>
</tr>
<tr>
<td>E, GPa</td>
<td>315</td>
<td>385</td>
<td>424</td>
<td>402</td>
<td>405</td>
</tr>
<tr>
<td>Kc, MPa⋅m^{1/2}</td>
<td>8.24</td>
<td>8.73</td>
<td>12.32</td>
<td>11.73</td>
<td>10.35</td>
</tr>
<tr>
<td>K_o</td>
<td>0</td>
<td>0.08</td>
<td>0.61</td>
<td>0.13</td>
<td>1.57</td>
</tr>
<tr>
<td>H_μ/E_2, GPa</td>
<td>0.143</td>
<td>0.315</td>
<td>0.351</td>
<td>0.329</td>
<td>0.304</td>
</tr>
</tbody>
</table>

It is found out that compared to TiN, multi-element coatings have a greater X-ray line half-width, greater residual compressive stresses, smaller CSR, and greater relative microdeformations of the crystal lattice. Comparing bi- and tri-element coatings shows that the latter have higher residual compressive stresses, whereas TiNbAlN has the greatest value of σ₀.

The half-width of the X-ray line depends on the design of cathodes and the layout of the machine used to apply the coating. β_{111} is at highest for TiZrAlN applied with solid titanium and zirconium cathodes; such coatings have a multi-layer structure. The absence of thereof in TiZrCrN is what results in lower β_{111}. These data accord to what is described in [6, 16]. Multi-layer TiZrAlN coatings also have the smallest SCR D and the greatest value of Δа/а.

Multi-element coatings have higher mechanical properties compared to TiN, see Table 2. Their microhardness is 1.48-1.64 times higher, and the modulus of elasticity is 1.2-1.35 times higher depending on the composition. Tri-element coatings have higher microhardness, modulus of elasticity, and fracture toughness, but lower adhesion strength compared to bi-element coatings. TiZrCrN have the least adhesion strength, whereas its stratification coefficient is considerably higher than that of other three-element coatings. Multi-element coatings do not differ significantly in terms of resistance to plastic deformation (the ratio H_μ/E_2). These data are in line with what is described in [6, 16], which is due to the effect of various mechanisms strengthening the material upon their condensation.
mechanical properties and residual stresses to generate higher normal compressive stress during cutting.

Based on these data and the principle of how multi-layer coatings are formed for continuous cutting, we have developed double-layer coatings where the lower level is TiZrN and the upper level is TiNbAIN, TiZrAIN, TiZrCrN. The efficiency thereof was tested by turning 38XTH steel workpieces. Figure 2 presents the results. It has been found out that use of our bi-layer coatings prolongs the tool life of carbide plates 1.8-2.8 times compared to TiN (the exact value depends on the cutting parameters and the material machined). In such terms, the most efficient coating is the double-layer with a TiNbAIN upper layer, the least efficient is that with TiZrCrN upper layer. TiZrN-TiZrCrN being less efficient is due to the lower adhesion strength of the lower layer as well as due to lower mechanical properties and residual compressive stresses characteristic of coatings made by composite cathodes [1, 2].

4 Conclusion

Multi-layer coatings improve the tool life of carbide tools compared to single-layer coatings. The most efficient are the coatings where the upper layer gives a favorable combination of mechanical properties and residual compressive stresses while the lower layer immediately adjacent to the tool has sufficient adhesion strength.

References


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