

The multi-objective genetic algorithm optimization, of a superplastic forming process, using ansys®

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Abstract: In the industrial practice, the product is intended to be flawless, with no technological difficulty in making the profile shapes. If this product results without defects, then any Finite Elements Method (FEM) based simulation can support that technology. A technology engineer does not propose, very often to analyze the simulation of the design technology, but rather to try to optimize a solution that he feels feasible. Experiments used as the basis for numerical optimization analysis support their research in the field of superplastic forming. Determining the influence of input parameters on the output parameters, Determining the optimal shape of the product and the optimal initial geometry, the prediction of the cracks and possibly the fractures, the prediction of the final thickness of the sheet, these are the objectives of the research and optimization for this project. The results of the numerical simulations have been compared with the measurements made on parts and sections of the parts obtained by superplastic forming. Of course, the consistency of the results, costs, benefits, and times required to perform numerical simulations are evaluated, but they are not objectives for optimizing the superplastic forming process.

1 Introduction

The engineering design system is an extremely laborious and delicate interdisciplinary process that requires co-operation between designers in various engineering fields. This means the technological design is considered to be a complex process and needs to be approached very carefully. Design engineering requires hypotheses that need to be adopted for the further development of models that can undergo analysis, verification, and experiments. The project starts, always with the analysis of several variants. For most applications, the entire design project can be subdivided into different subproblems that can then be independently addressed. Each subproblem can thus be presented as a design optimum to be mathematically solved, M. Diehl, F. Glineur, E. Jarlebring, W. Michiels [1].

For technology engineers to apply optimization methods to a project, they need to have a detailed understanding of both theory and algorithms and their specific techniques. This is due, first of all, to the fact that considerable effort is needed to apply optimization techniques to practical problems to achieve an improvement in the performance of the studied product. For this reason, perhaps, optimization has been used, in

particular, to help the projection process, namely to support decision-making, not to develop concepts, or to develop a detailed project.

Generally, for technology engineers, optimization issues are reduced to minimization a function (a cost function, for example), or maximizing a function (a "profit" function), a function that is subject to constraints (mathematically, these may be some inequalities or equations), the optimization problem being called the nonlinear programming problem. Its general form is, A. D. Belegundu and T. R. Chandrupatla [2]:

Minimize:

$$\mathbf{f}(\mathbf{x}, \mathbf{y}) \quad (1)$$

subject to:

$$\mathbf{g}_i(\mathbf{x}, \mathbf{y}) \leq \mathbf{0} \quad i = 1, \dots, m \quad (2)$$

$$\mathbf{h}_j(\mathbf{x}, \mathbf{y}) \geq \mathbf{0}, \quad j = 1 \dots \ell \quad (3)$$

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where

$$\mathbf{x} \in \mathbb{R}^{n_c}, \mathbf{y} \in \mathbb{R}^{n_i}$$

$$\mathbf{x}_l \leq \mathbf{x} \leq \mathbf{x}_u$$

$$\mathbf{y}_l \leq \mathbf{y} \leq \mathbf{y}_u$$

Not often (it can be said that this is the real challenge for an engineer regarding a genuinely delicate optimization problem), both a minimization and a maximization may be required, of course, on various criteria, clearly set, the problem is extremely complex and cost-generating. For example, a structural engineer may like to minimize the mass of the product, but would also like to increase mechanical rigidity. At this point, several goals can be discussed simultaneously. Mathematically, the problem with multiple targets (or "attributes") may be stated as, A. D. Belegundu and T. R. Chandrupatla [2]:

$$\text{minimize } \mathbf{f} = [\mathbf{f}_1(\mathbf{x}), \mathbf{f}_2(\mathbf{x}), \dots, \mathbf{f}_m(\mathbf{x})]$$

$$\text{subject to } \mathbf{x} \in \Omega$$

When, very rarely, it happens that only one optimum criterion \mathbf{x}_{opt} minimizes all the objectives, the problem is solved instantly. Most of the time, however, the optimization criteria are in conflict. In this situation, the optimization problem is solved by weighting the criteria:

$$\text{minimize } \mathbf{f} = \omega_1 \mathbf{f}_1(\mathbf{x}) + \omega_2 \mathbf{f}_2(\mathbf{x}) + \dots$$

$$\text{subject to } \mathbf{x} \in \Omega$$

where the weights ω_i are positives, and $\sum \omega_i = 1$. Choosing the sizes of these weights is based on experimental data.

Another approach, quite common, is to designate one of the criteria as a priority, and to constrain the values for the weights of the other criteria:

$$\text{minimize } \mathbf{f}_1(\mathbf{x})$$

$$\text{subject to } \mathbf{f}_2(\mathbf{x}) \leq \mathbf{c}_2$$

...

$$\mathbf{f}_m(\mathbf{x}) \leq \mathbf{c}_m$$

$$\mathbf{x} \in \Omega$$

Even if the use of a set of values for weights, ω_i , or limits, \mathbf{c}_i , generates an optimum, \mathbf{x}_{opt} , that corresponds to all criteria, an engineer must be able to answer the question, what if the different selection of set of values will done, the results are different? Then comes the answer: we must take into account the sensitivities of the output parameters with respect to the input parameters, and the Parameters Correlation, the computation and

optimization module, provided by ANSYS as a feature, mathematics and graphics at the same time.

2 Optimization procedure

The studied part, shown in Fig. 1, is hemispherical with flange, G. Grebenişan and S. Mureşan [3]. The blank is fixed, with friction, between the two components of the forming die, on its perimeter and the entire assembly is heated in a horizontal oven, for superplastic forming at high temperature (under the half of melting temperature of the material, i.e. approximately 460[°C], for Supral 100, commercial named, this Aluminium alloy. The gas pressure will act and deform the sample, with a very low strain rate $\dot{\epsilon} = 2.5 \times 10^{-3} [s^{-1}]$. The material is modeled with an Anand Viscoplasticity law as described by M.M. Rahman [4]. The strain distribution on the workpiece section and resultant thickness of the specimen it's possible to be very variable from one area to another, leading to a nonhomogeneous thickness distribution in the final component. This will also induce higher stress zones. The authors J.-P. Ponthot, J.-P. Kleinermann [5] proposed an approach to avoid these problems. The mentioned authors proposed to use the following procedure: to determine the initial piece geometry that would lead, at the end of forming process, to the prescribed uniform distribution of the thickness of the final workpiece transversal section. Furthermore, we chosen as input parameters the sample diameter and the thickness of the sample.



a)-hemispherical parts



b)-hemispherical (midsection and quarter section)

Fig. 1. Studied parts

Later, in this workpaper, a Design of Experiments(DOE) is presented and is easy to found that the study involves a sampling point which not always conducive to lowering the time needed for the analysis.

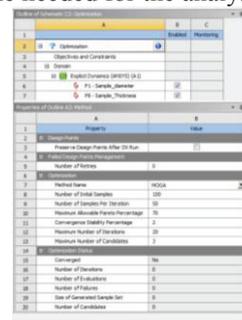


Fig. 2. The Settings of Direct Optimization

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Table 1. Raw optimization data

Nam e	P1 - Sampl e_dia meter (mm)	P8 - Sampl e_Thic kness (mm)	P5 - Equivale nt Stress Maximu m (MPa)	P6 - Total Deforma tion Maximu m (mm)	P7 - Equivale nt Plastic Strain Maximu m (mm mm^-1)
1	18.02	1.08	488.91	15.08	0.24
2	18.06	1.20	495.75	15.31	0.22
3	18.10	1.14	484.52	15.22	0.22
4	18.14	1.26	485.42	15.44	0.24
5	18.18	1.11	494.11	15.20	0.22
6	18.22	1.23	535.34	15.38	0.22
7	18.26	1.17	499.01	15.30	0.22
8	18.30	1.29	517.91	15.15	0.23
9	18.34	1.10	491.14	15.25	0.22
10	18.38	1.22	554.64	15.19	0.23
11	18.42	1.16	466.27	15.15	0.23
12	18.46	1.28	476.75	15.13	0.25
13	18.50	1.13	533.48	15.34	0.24
14	18.54	1.25	505.48	15.24	0.24
15	18.58	1.19	520.15	15.14	0.24
16	18.62	1.31	433.10	15.16	0.25
17	18.66	1.09	513.64	15.35	0.25
18	18.70	1.21	484.48	15.06	0.24
19	18.74	1.15	466.67	15.09	0.25
20	18.78	1.27	492.00	15.10	0.73
21	18.82	1.12	470.99	15.13	0.27
22	18.86	1.24	522.50	15.04	0.26
23	18.90	1.18	538.05	15.19	0.25
24	18.94	1.30	723.67	15.09	0.73
25	18.98	1.10	468.50	15.10	0.27
26	19.02	1.22	612.17	15.11	0.26
27	19.06	1.16	441.66	15.08	0.26
28	19.10	1.28	667.51	15.04	0.73
29	19.14	1.13	604.14	15.25	0.27
30	19.18	1.25	462.46	15.14	0.27
31	19.22	1.19	560.77	15.24	0.27
32	19.26	1.31	654.86	15.33	0.65
...
371	20.95	1.31	748.18	15.24	0.43
372	21.98	1.32	702.80	15.21	0.70
373	21.44	1.26	775.84	15.16	0.57
374	21.77	1.29	707.99	15.20	0.68

For example, applying a CCD in a fractional factorial scheme, a dozen times more sampling points are required for some input parameters, that is, as many evaluations as Finite Element Analysis, which means a significant computational time is consuming, G. Gantar, T. Pepelnjak, K. Kuzman [6].

The MOGA method (Multi-Objective Genetic Algorithm), fig. 2, is a variant of the popular Non-dominated Sorted Genetic Algorithm-II (NSGA-II) based on controlled elitism concepts. It supports multiple objectives and constraints and aims at finding the global optimum, Ansys manual [7].

The method's Configuration is: will generate 100 samples initially, 50 samples per iteration and find 3 candidates in a maximum of 20 iterations, fig. 3.

1	Optimization Study	A	B	C	D
2	Seek P7 = 0.6 mm mm^-1; 0.2 mm mm^-1 <= P7 <= 1 mm mm^-1				Goal, Seek P7 = 0.2 mm mm^-1 (Default Importance); Strict Constraint, P7 values between 0.2 mm mm^-1 and 1 mm mm^-1 (Default Importance)
3	Maximize P5; P5 <= 900 MPa				Goal, Maximize P5 (Default Importance); Strict Constraint, P5 values less than or equals to 900 MPa (Default Importance)
4	Maximize P8				Goal, Maximize P8 (Default Importance)
5	Optimization Method				
6	MOGA				The MOGA method (Multi-Objective Genetic Algorithm) is a variant of the popular NSGA-II (Non-dominated Sorted Genetic Algorithm-II) based on controlled elitism concepts. It supports multiple objectives and constraints and aims at finding the global optimum.
7	Configuration				Generate 100 samples initially, 50 samples per iteration and find 3 candidates in a maximum of 20 iterations.
8	Status				Converged after 374 evaluations.
9	Candidate Points				
10		Candidate Point 1	Candidate Point 2	Candidate Point 3	
11	P1 - Sample_diameter (mm)	20.946	21.971	21.598	
12	P8 - Sample_Thickness (mm)	1.3129	1.3129	1.3129	
13	P5 - Equivalent Stress Maximum (MPa)	775.45	744.74	775.12	
14	P7 - Equivalent Plastic Strain Maximum (mm mm^-1)	0.59799	0.60308	0.54843	

Fig. 3. Table of Schematic C2: Optimization(Optimization Study; Optimization Method; Candidate Points)

Our application was realized after 4 hours of computing time; the results are concentrated on four modules: Candidate Points, Tradeoff, Samples, and Sensitivities. The method converged after 374 Design Points evaluated(Table 1).

1	Optimization	Enabled	Monitoring
2	Optimization		
3	Objectives and Constraints		
4	Maximize P5; P5 <= 900 MPa		
5	Seek P7 = 0.6 mm mm^-1; 0.2 mm mm^-1 <= P7 <= 1 mm mm^-1		
6	Maximize P8		
7	Domain		
8	Explicit Dynamics (ANSYS) (A1)		
9	P1 - Sample_diameter	<input checked="" type="checkbox"/>	
10	P8 - Sample_Thickness	<input checked="" type="checkbox"/>	
11	Parameter Relationships		
12	Raw Optimization Data		
13	Convergence Criteria		
14	Results		
15	Candidate Points		
16	Tradeoff		
17	Samples		
18	Sensitivities		

Fig. 4. Outline of Schematic C2: Optimization

3 Results of the Multi-Objective Genetic Algorithm (MOGA)

1	A	B	C	D	E	F	G	H	I	J
2	Reference	Name	P1 - Sample_diameter (mm)	P8 - Sample_Thickness (mm)	P5 - Equivalent Stress Maximum (MPa)	P7 - Total Deformation Maximum (mm mm^-1)	P7 - Equivalent Plastic Strain Maximum (mm mm^-1)			
3		Candidate Point 1	20.946	1.3129	775.45	0.598	0.59	0.94		
4		Candidate Point 2	21.971	1.3129	744.74	0.603	0.60	0.96		
5		Candidate Point 3	21.598	1.3129	775.12	0.548	0.54	0.00		
6		New Custom Candidate Point	21	1.2						

Fig. 5. Table of Schematic C2: Optimization, Candidate Points

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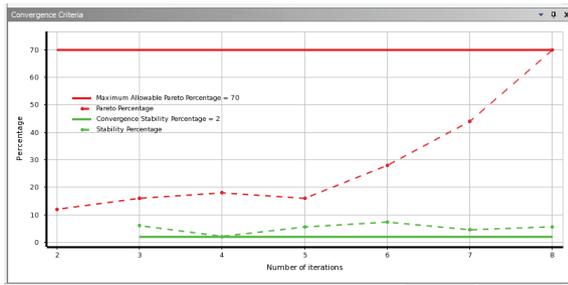


Fig. 6. Convergence Criteria

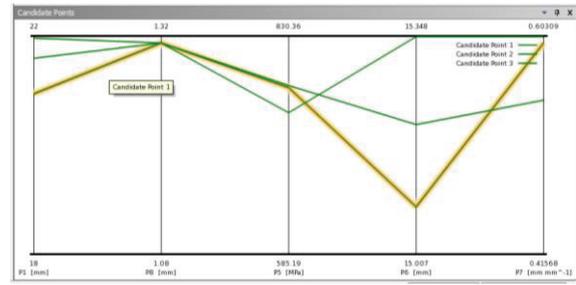


Fig. 11. Candidate Points

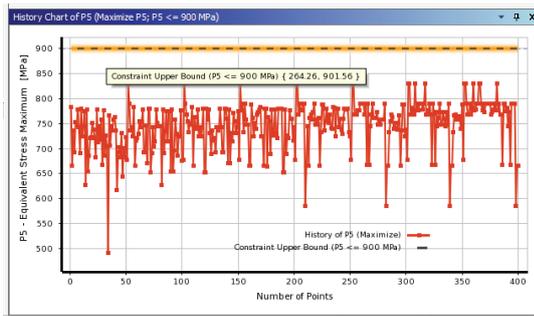
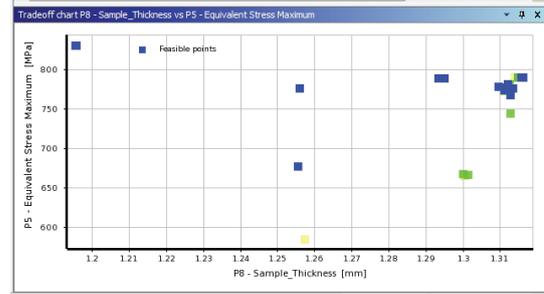


Fig. 7. History Chart of parameter P5 (Maximize P5- Equivalent Stress Maximum)



a)- Sample_Thickness vs. Equivalent Stress Maximum

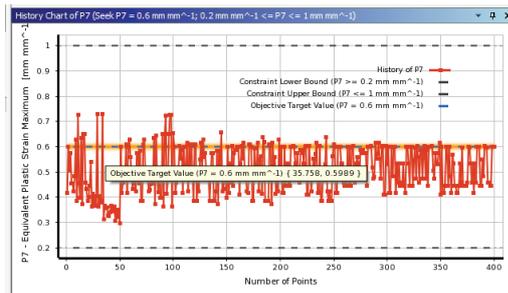
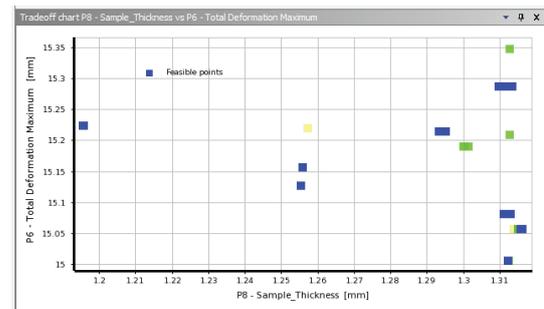


Fig. 8. History Chart of parameter P7 (Seek P7- Equivalent Plastic Strain Maximum)



b)- Sample_Thickness vs. Total Deformation Maximum

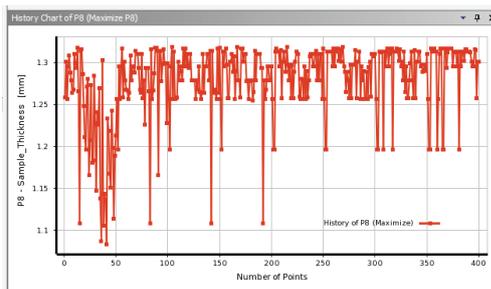
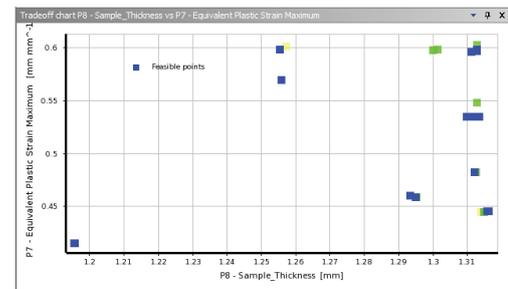


Fig. 9. History Chart of parameter P8 (Maximize P8- Sample_Thickness)



c)- Sample_Thickness vs Equivalent Plastic Strain Max.

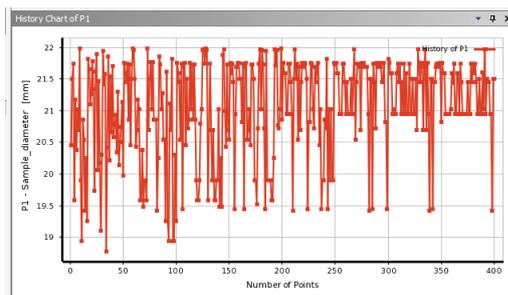
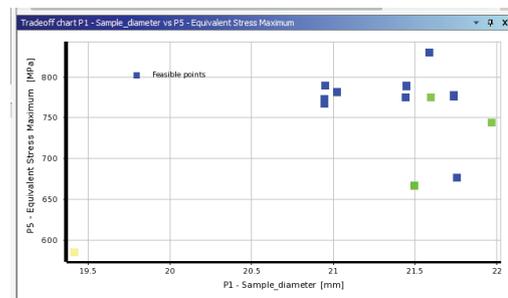
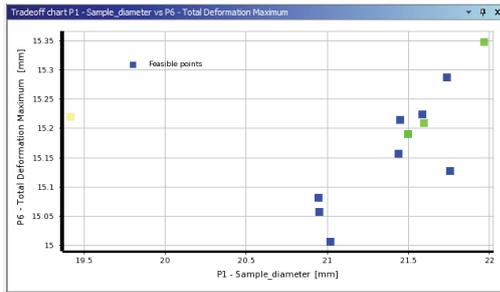


Fig. 10. History Chart of parameter P1 (Sample_diameter)

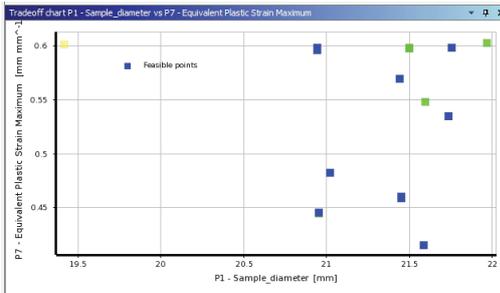


d)- Sample_diameter vs Equivalent Stress Maximum

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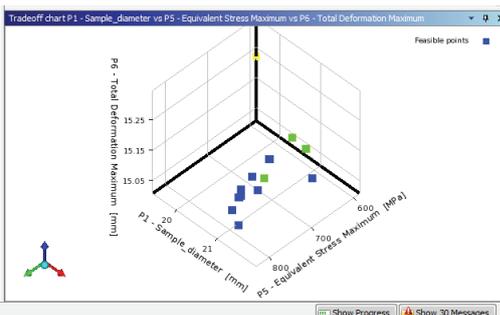


e)- Sample_diameter vs Total Deformation Maximum

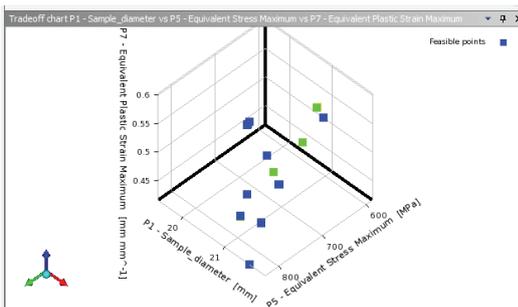


f)- Sample_diameter vs Equivalent Plastic Strain Max.

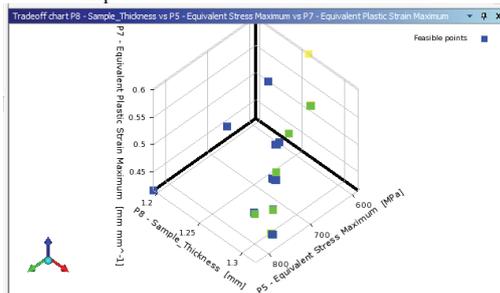
Fig. 12. Tradeoff-feasible points-2D



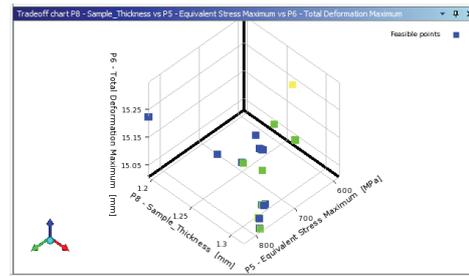
a)- Sample_diameter vs Equivalent Stress Maximum vs Total Deformation Maximum



b)- Sample_diameter vs Equivalent Stress Maximum vs Equivalent Plastic Strain Maximum



c)- Sample_Thickness vs Equivalent Stress Maximum vs Equivalent Plastic Strain Maximum



d) - Sample_Thickness vs. Equivalent Stress Maximum vs. Total Deformation Maximum

Fig. 13. Tradeoff-feasible points-3D

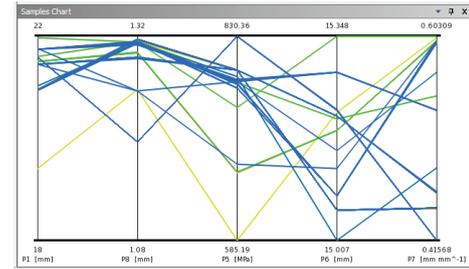


Fig. 14. Samples Chart

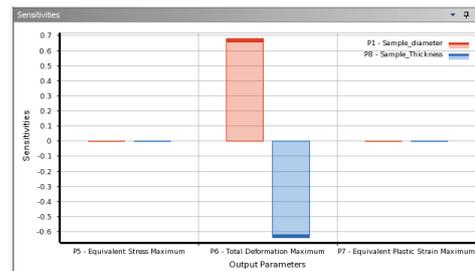


Fig. 15. The Sensitivities of output parameters with respect on input parameters

Response Surface created based on MOGA Optimization are:

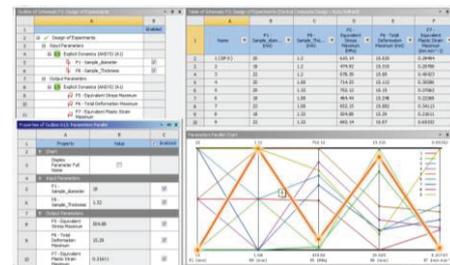


Fig. 16. Design of Experiments(Central Composite Design) and Parameters Parallel Chart

1	Name	P1 - Equivalent Stress Maximum	P6 - Total Deformation Maximum	P7 - Equivalent Plastic Strain Maximum
2	Standard of Fit			
3	Coefficient of Determination (R-Square Value = 0.7)	0.88708	0.8822	0.99953
4	Adjusted Coefficient of Determination (R-Square Value = 0.7)	0.83811	0.84293	0.99874
5	Maximum Relative Residual (Mean Value = 0%)	13.445	0.4688	1.8332
6	Least Squares Square Error (Mean Value = 0%)	36.474	0.024022	0.0028364
7	Root Mean Square Error (Mean Value = 0%)	6.039	0.23828	1.3746
8	Relative Maximum Absolute Error (Mean Value = 0%)	77.89	66.413	3.9076
9	Relative Average Absolute Error (Mean Value = 0%)	25.512	23.975	1.4734

Fig. 17. Table of Outline A14: Goodness Of Fit

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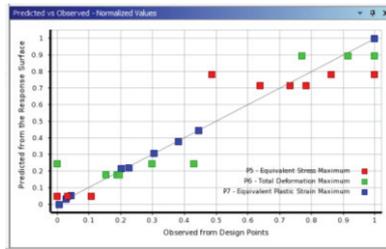
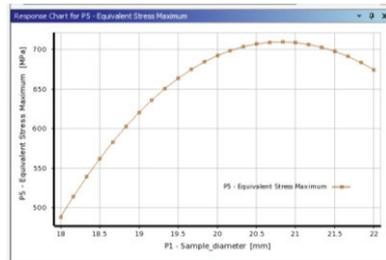
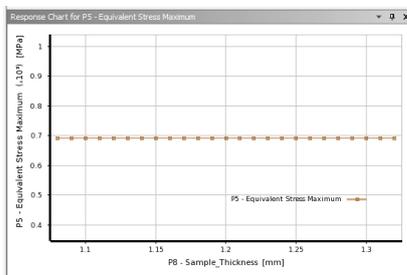


Fig. 18. Goodness of fit for Predicted Point vs. Observed Point

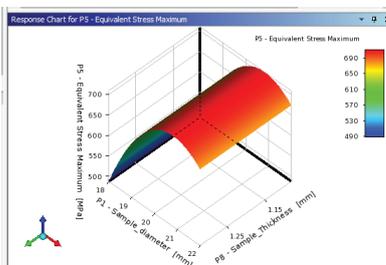


a) Sample_diameter vs Equivalent Stress Maximum

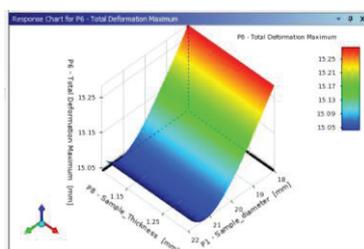


b)- Sample_Thickness vs. Equivalent Stress Maximum

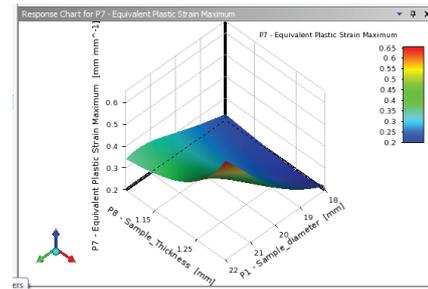
Fig. 19. Response Surface(2D)



a)-Sample_diameter vs. Sample_Thickness vs. Equivalent Stress Maximum



b)- Sample_diameter vs. Sample_Thickness vs. Total Deformation Maximum



c)- Sample_diameter vs. Sample_Thickness vs. Equivalent Plastic Strain Maximum

Fig. 20. Response Surface(3D)-Equivalent Stress Maximum

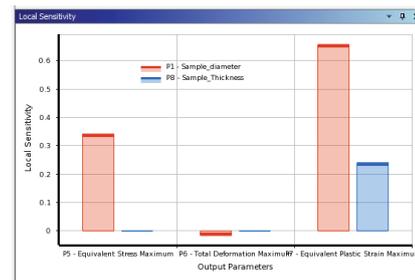


Fig. 21. Local Sensitivity of output parameters with respect to input parameters

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