

Outdoor Performance Comparison of Concentrator Photovoltaic and Flat Plate Photovoltaic Systems

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Abstract. Output characteristics of tracking type concentrator photovoltaic (CPV) system, multi-crystalline silicon (mc-Si) PV system, CIGS PV system, and amorphous silicon (a-Si) PV system were analyzed in the data period of a year from August 2013 to July 2014. In this study, we analyzed the influence of environmental factors using average photon energy (APE) and temperature of solar cell (T_{cell}). The characteristics of 14 kW CPV system, 50 kW mc-Si PV system, 60 kW CIGS PV system, 1.35 kW a-Si PV system were evaluated and compared. As a result, the output performance of CPV was highest between the four systems at the most frequent conditions in the outdoor environment.

1 Introduction

Multi-junction solar cells have attracted increasing attention for application in concentrator photovoltaic (CPV) system owing to their very high conversion efficiency [1]. Multi-junction solar cells consisting of InGaP, InGaAs, and Ge diodes are recognized as super high efficiency cells and are used for space application. Light concentration is one of the most important factors for the development of an advanced PV system using high-efficiency solar cells. High-efficiency multi-junction cells under high light concentration have been investigated for terrestrial application [2,3].

In Japan, there are a few reports in field-test data of CPV systems. Therefore, it is important to accumulate the field-test data of CPV systems and evaluate them. PV systems which are generally used are crystalline-silicon (c-Si) PV system, CIGS PV system and amorphous silicon (a-Si) PV system.

The conversion efficiency of solar cell decreases with increasing temperature [4,5]. Characteristics of CPV are more sensitive to spectrum as compared to flat-plate PV because CPV systems use lens and multi-junction solar cells.

In this study, we analyzed the influence of environmental factors in Japanese meteorological conditions using an index of average photon energy (APE) and temperature [6]. Moreover, we compared CPV, multi-crystalline silicon (mc-Si) PV, CIGS PV, a-Si PV.

2 Experimental Procedure

Fig.1 (a) shows a 14 kW CPV system (Daido Steel Co., Ltd.) installed in the University of Miyazaki. Panel area was 7 m × 10 m. A Fresnel lens (160 mm × 160 mm)

concentrates sunlight and concentrated light is irradiated onto a triple-junction solar cell (7 mm × 7 mm). A CPV module was fabricated by connecting 25 lens-cell pairs in series. The 14 kW CPV system is composed of 96 modules. Fig.1 (b) shows a 50 kW multi-crystalline Si (flat plate) PV system. The panel area of this system was 381 m². Fig.2 (c) shows a 60 kW CIGS (flat-plate) PV system. The panel area of this system was 563 m². Fig.2 (d) shows a 1.35 kW a-Si (flat-plate) PV system. The panel area of this system was 22 m². These 50 kW mc-Si PV system, 60 kW CIGS PV system and 1.35 kW a-Si PV system were also installed in the same site.



Figure 1. CPV and flat plate systems installed in University of Miyazaki.

As meteorological data, we measured direct normalized irradiance (DNI), global irradiance (GI), direct solar spectra, and global solar spectra every 1

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minute. DNI and GI were respectively measured by the DNI meter and GI meter. The solar spectrum was measured with the wavelength range from 350 to 1050 nm, the solar spectrum was recorded every 1 minute by a spectro-radiometer (MS700, EKO). Direct solar irradiance was recorded by a spectro-radiometer with a collimation tube (aperture angle:±2.5°).

APE is an index that indicates a spectral irradiance distribution [6]. A value of APE was calculated from measured value of spectral irradiance by dividing the integrated irradiance with the integrated photon flux density, yielding the average energy per photon(eV):

$$APE = \frac{\int_a^b E(\lambda) d\lambda}{q \int_a^b \Phi(\lambda) d\lambda} \quad (1)$$

where q is the electronic charge, E spectral irradiance and Φ the spectral photon flux density, respectively. For the limitation of our measurement system, a and b were set to 350 and 1050 nm, respectively. For the CPV system, Fig. 2 shows a flow chart of how the contour graphs were made from APE, T_{cell} , output energy (P_{out}), and DNI, respectively. The methodology is as follows:

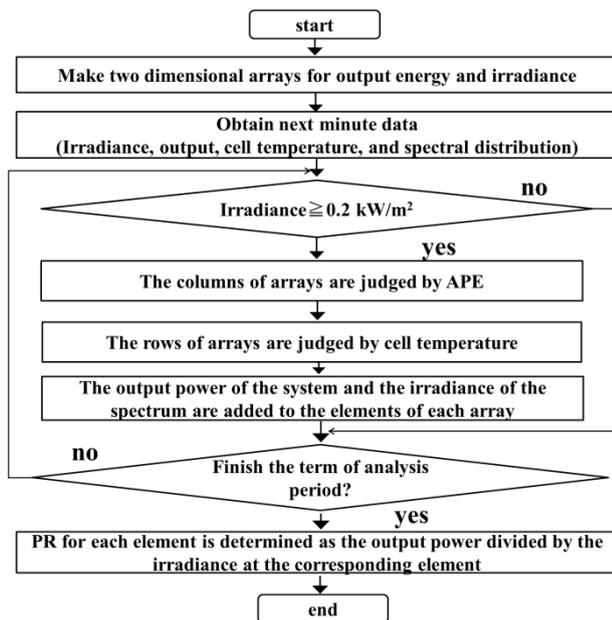


Figure 2. Flow chart of how the contour map was made.

(1) The data of T_{cell} , DNI for 1 m^2 , P_{out} of the system which has nominal output power of 14kW, and the spectral irradiance distribution at the analysis period are prepared. The two-dimensional arrays for DNI and for P_{out} are prepared. The arrays for P_{out} and DNI have APE (1.80-1.99eV, 0.01 eV step) and T_{cell} (0-80°C, 5°Cstep) for column and row, respectively.

(2) The following steps are repeated for the data measured every 1 minute from August 2013 to July 2014. Here, the data with DNI higher than 0.20 kW/m^2 were used and lower performance of system at low DNI was omitted. The reason why we used irradiance higher than 0.20 kW/m^2 was the fluctuation of output voltage, which resulted in fluctuation of the maximum power point tracking (MPPT) control of the inverter.

(a) APE of spectrum is determined by the spectrum distribution.

(b) The columns of both P_{out} and DNI arrays for the spectrum are indexed by APE.

(c) The rows of both P_{out} and DNI arrays for the spectrum are indexed by T_{cell} . Then, the elements of the arrays for the spectrum are determined.

(d) P_{out} of the system and DNI of the spectrum are added to the elements of each array.

(3) Performance ratio (PR) is determined as P_{out} divided by DNI at the corresponding element. PR is given as follows:

$$PR = \frac{\frac{P_{out} \text{ (kW)}}{DNI \text{ (kW/m}^2)}}{\frac{P_{max} \text{ (kW)} [\text{rated power of CPV system}]}{1 \text{ (kW/m}^2)} [DNI \text{ for rating}]} \quad (2)$$

where P_{max} is the nominal maximum output power under the standard test condition. For the mc-Si, CIGS and a-Si systems, the same method was used for making contour map. GI and solar spectrum without collimation tube were used.

3 Results and Discussion

Figure 3 shows the contour maps of PR of CPV, mc-Si PV, CIGS PV, a-Si PV systems as function of APE and T_{cell} . In the case of mc-Si, the value of PR decreases with increasing temperature owing to decrease of open-circuit voltage (V_{oc}) [7]. In the case of CPV, the decrease of PR with increasing temperature gets balanced out with the increase of performance owing to the high DNI [8].

In the case of CIGS, the value of PR decreases with increasing T_{cell} as mc-Si when APE was more than 1.90 eV. However, PR decreases with decreasing APE when APE was less than 1.88 eV. In the case of a-Si, the value of PR increases with increasing temperature owing to anneal effect [9].

Table 1 shows the most frequent conditions for the four systems and the value of PR in four systems at these conditions.

The PR of CPV at most frequent condition had the highest value.

These results indicated that the importance of the understanding of the behavior of the outdoor performance in various PVs and the accurate data of environmental conditions where various PVs are installed.

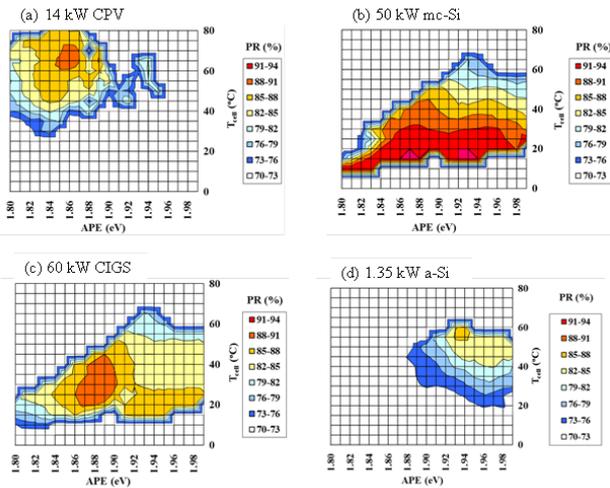


Figure 3. The outdoor performance of CPV and flat plate systems as function APE and T_{cell}

Table 1

The value of PR at the most frequent conditions in four systems

	CPV	mc-Si	CIGS	a-Si
Most frequent condition (APE(eV), T_{cell} (°C))	1.830 ± 0.005 , 60 ± 5	1.920 ± 0.005 , 45 ± 5	1.920 ± 0.005 , 45 ± 5	1.920 ± 0.005 , 40 ± 5
PR (%)	86	84.5	84.3	77.3

4 Conclusion

We analyzed the influence of environmental factors in Japanese meteorological conditions using an index of average photon energy (APE) and temperature. Outdoor performance characteristics of four systems were different. The CPV and mc-Si PV systems were depended to APE and cell temperature, respectively. However, the characteristic of CIGS PV system was intermediate between CPV and mc-Si. The value of PR of CPV at the most frequent condition was higher than others. The characteristic of a-Si PV system increased owing to anneal effect.

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