

The Effect of Different Sintering Strategies on Properties of YSZ Reinforced Graphene Composites

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Abstract. Partial, single and double step sintering has been carried out to densify YSZ reinforced 1 wt. % graphene composites at temperature as low as 40% of the homologous temperature. The influence of sintering conditions on resulting density, microstructure, porosity and contact angles were determined. The microstructure of the composites showed that amount of micro pores was reduced upon double step sintering and infiltrating with PDC resin. This study has improved upon existing sintering methods resulting in the use of low temperature for sintering ceramics yet achieving relative density >95% with porosity as low as 0.15 using double step sintering.

1 Introduction

Sintering is a complicated microstructure evolution process; wherein the major aim is porosity elimination [1–3]. As such, the major aim of this study is to shed light and investigate the influence of various sintering strategies (partial step sintering, single step sintering and double step sintering) on the porosity elimination of ceramics. Hence, main attention is addressed in the relative density, grain size, pore size and percentage porosity of YSZ reinforced graphene-composite which are ideally well suited for manufacturing of engineering components subjected to large mechanical stresses and extreme conditions such as hostile environments and high temperatures [4]. Besides, temporal variations on the surface energy of the ceramic were studied using a goniometer.

2 Experimental procedures

2.1 Preparation of Ceramic Suspension

The procedure for preparation of YSZ reinforced graphene suspension has been reported previously [5]. In short, Ytria Stabilised Zirconia (YSZ) reinforced with 1 wt. % graphene was used as the structural material; where the green bodies were obtained by gel-casting on PDMS soft molds.

2.2 Sintering Mechanism

Different strategies were implemented to densify the composite of the green body; (a) single step sintering at temperature of 1200°C for 4 hours; (b) double step sintering by ramping the temperature to 1200°C,

reduced immediately to 900°C and held for 30 hours (c) partial sintering at lower temperature of 900°C for 2 hours. After natural cooling to room temperature, the ceramics were removed and immersed into a polymer derived ceramic (PDC) resin (RD-212a, Starfire Systems Inc.) for an hour followed by thermal curing of the resin at 250°C for an hour. The ceramics were reheated for 2 hours at 900°C for conversion of the resin into SiOC ceramic.

2.3 Characterizations

The bulk density of all samples was determined via Archimedes method using a pycnometer (Laborglass, Germany). Porosity of the ceramics were determined using Eq. 1;

$$Porosity = \left[1 - \left(\frac{\rho_{bulk}}{\rho_{theoretical}} \right) \right] \times 100 \% \quad (1)$$

Where ρ_{bulk} is the bulk density of the ceramic composite (g/cm³) and $\rho_{theoretical}$ is the theoretical density of the ceramic composites (g/cm³). A contact angle goniometer (Model 250, Rame-Hart) was used to measure the contact angle between the liquid droplets and sintered YSZ-graphene surface. Microstructures of YSZ-graphene composites fabricated via different sintering mechanisms were investigated using high-resolution SEM (SEM, Quanta400F, FEI).

3 Results and discussion

The effect of different sintering strategies on the relative density, grain size, pore size and porosity are as

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depicted Figure 1. It indicates that porosity decreases as relative density increases and pore size decreases as grain size increases. Furthermore, porosity variation is due to YSZ grain size upon various sintering mechanisms. The porosity after double step sintering was reduced for YSZ particles in comparison to that of single step sintering or partially sintering. This phenomenon is due to improved compressibility of particles upon double step sintering, leading to grain growth. Higher relative density was achieved at higher temperature; partial step sintering at 900°C (rel. density

93%), single and double step sintering at 1200°C (rel. density 94.1 and 95.4% respectively). As shown in Eq. (2), the rate of diffusion depends on the sintering temperature. As such, denser structure is achieved at higher sintering temperature.

$$D = D_0 \exp\left(\frac{-Q}{RT}\right) \quad (2)$$

Where D is the diffusion coefficient, D₀ is the constant, Q is the activation energy, R is Boltzmann constant and T is the temperature.

Table 1. Properties of composite after various sintering

Processing	Relative density (%)	Grain size (nm)	Average pore size (nm)	Porosity (%)
Partial	93	167±18	126±13	23.3
Single	94.1	186±21	98±16	16.7
Double	95.4	194±16	76±17	15.1

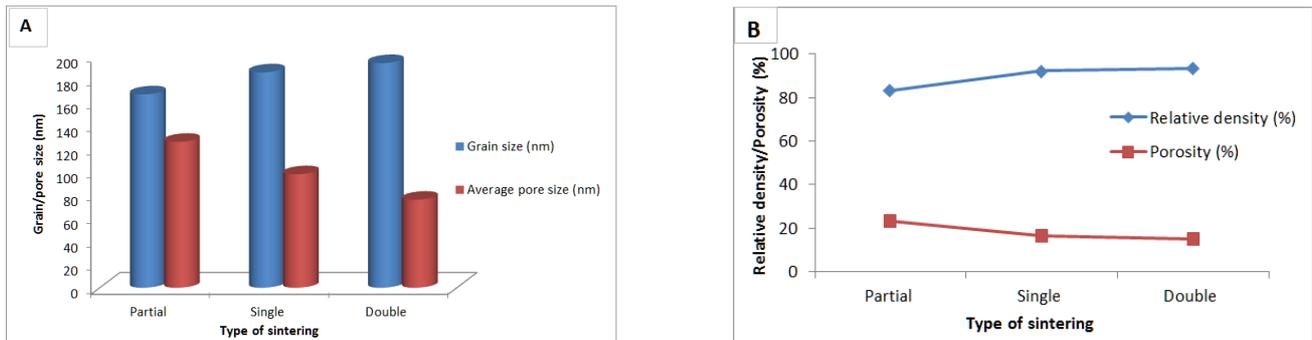


Figure 1. Effect of various sintering on (a) relative density and porosity of ceramic (b) grain and pore size.

Besides, it should be noted that sintering time of double step sintering was relatively high (30 hours) in comparison to single step sintering (4 hours) and partial step sintering (2 hours). The evolution of microstructure with sintering time is as depicted in Figure 2. The dependence of the diffusion to time can be explained by Eq. (3),

$$r = 2.4\sqrt{Dt} \quad (3)$$

Where r is radical distance, D is the diffusion coefficient and t is the sintering time. It can be seen that atomic displacement is proportional to the square root of time. This is responsible for atomic diffusion which leads to grain coarsening. Thus, the manifestation of Eq. (3) can be clearly seen by the changes in morphology and the size of pores and grains.

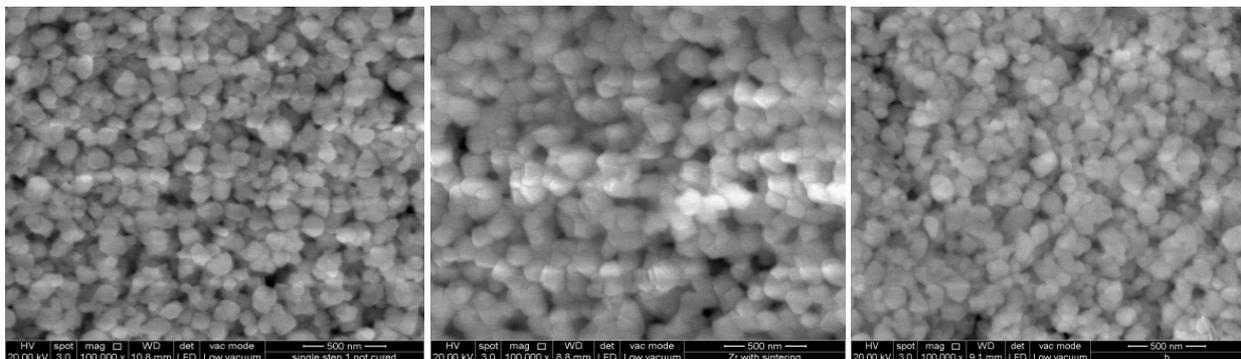


Figure 2. SEM images of YSZ reinforced with 1wt% graphene after (a) partial step sintering (b) single step sintering (c) double step sintering

Contact angle measurements on composites were used in an effort to determine the surface energies. Surface energies are important to understand the wetting and adhesion properties of materials. However, determining surface energy is not trivial whereas measuring contact angle is simpler. In this study, the contact angles of deionized water droplet on the ceramic surface are plotted against time for gradual decrement of angles as the liquid penetrates through the surface of the composite (Figure 3). It is observed that the composite fabricated via double step sintering has higher contact angle (>90°) in comparison to those via single step and partial step sintering respectively. This is attributed by the presence of lesser pores (quantity and size) that leads to contact angles greater than 90°; designated as hydrophobic surfaces.

Figure 4 shows the effect of different types of sintering on volume reduction of water droplet on ceramics. It is evident that the volume decreases more slowly with double step sintering compared to that of partial step sintering and single step sintering; partially

sintered composites has a steeper slope in comparison to single step sintered and double step sintered composites.

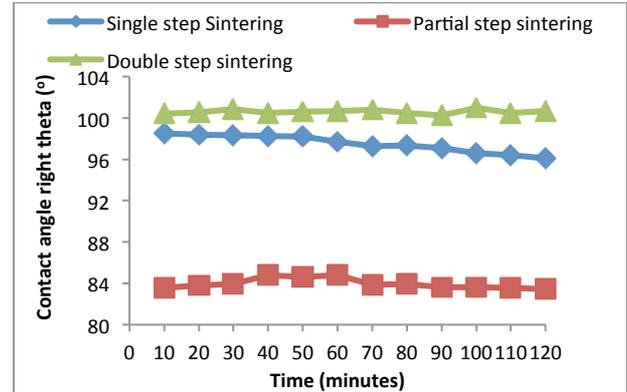


Figure 3. Effect of sintering on right theta

$$m_{\text{partial step sintering}} > m_{\text{single step sintering}} > m_{\text{double step sintering}}$$

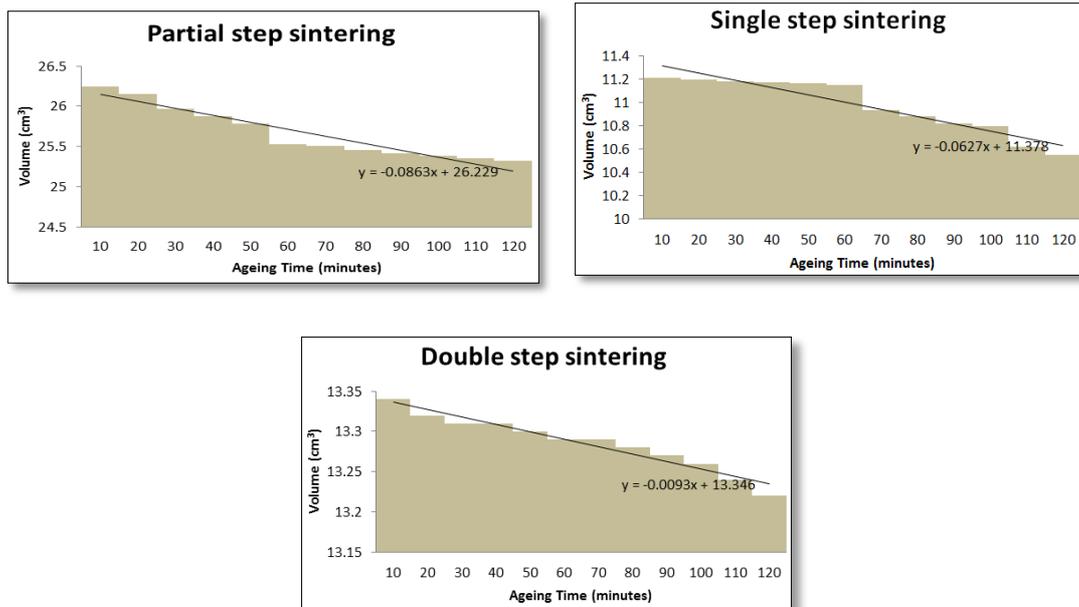


Figure 4. Effect of various sintering mechanism on volume reduction on ceramic surface.

4 Conclusion

The influence of different sintering mechanisms on the microstructure, density, porosity and contact angles was investigated. Experimental findings establish double step sintering as an effective sintering mechanism at low temperature yet achieving relative density >95% and low porosity (0.15) in comparison to partial or single step sintering.

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