

# An orthogonal technique for empirical mode decomposition in Hilbert-Huang transform

Menglin Lou<sup>1,a</sup> and Tianli Huang<sup>2</sup>

<sup>1</sup>Tongji University, School of Civil Engineering, Shanghai, China  
<sup>2</sup>Central South University, School of Civil Engineering, Changsha, China

**Abstract.** First, it is indicated that the intrinsic mode functions (IMF) obtained by the empirical mode decomposition (EMD) are not orthogonal. Then an orthogonal technique based on Gram-Schmidt method is proposed to obtain the complete orthogonal intrinsic mode functions. Three ways of the orthogonal processes are suggested and compared in the paper. Finally, the suggested method is validated through the decomposition of a typical time history. The numerical results show that the orthogonal IMF can be obtained easily by the technique proposed in the paper.

## 1 Intrinsic mode functions

Hilbert-Huang transform is applied widely in the signal analysis process as well as in Earthquake Engineering<sup>[1-3]</sup>. After the empirical mode decomposition (EMD), the signal  $X(t)$  can be expressed as

$$X(t) = \sum_{j=1}^n c_j(t) + r_n(t) \quad (1)$$

where  $c_j(t)$  is the  $j^{\text{th}}$  intrinsic mode function (IMF),  $r_n(t)$  is the residual function.

The integral orthogonal index  $IOT$  and the orthogonal index  $IO_{jk}$  between the  $j^{\text{th}}$  IMF and the  $k^{\text{th}}$  IMF are designated respectively for checking the orthogonality of the IMFs.

$$IOT = \sum_{j=1}^{n+1} \sum_{k=1}^{n+1} \int_0^T c_j(t)c_k(t)dt \bigg/ \int_0^T X^2(t)dt \quad (2)$$

$$IO_{jk} = \frac{\int_0^T c_j(t)c_k(t)dt}{\int_0^T c_j^2(t)dt + \int_0^T c_k^2(t)dt} \quad (3)$$

If all of IMFs are orthogonal mutually, the values of  $IOT$  and  $IO_{jk}$  are zero. However, the orthogonality of the IMFs can not be verified by mathematical technique. The following simple example shows the IMFs are not orthogonal. The signal  $X(t)$  is assumed as the sum of three sinusoidal waves

$$X(t) = \sum_{j=1}^3 x_j(t) = \sum_{j=1}^3 \sin(2\pi f_j t) \quad (4)$$

where  $f_1 = 1\text{Hz}$ ,  $f_2 = 5\text{Hz}$ ,  $f_3 = 10\text{Hz}$ . Its time history curve with 5 seconds is shown in Figure 1. Obviously, three sinusoidal waves are orthogonal, the theoretical values of  $IOT$  and  $IO_{jk}$  are zero. The numerical values of

$IOT$  and  $IO_{jk}$  are very small if they are calculated by computer, such as  $IOT = 2.5545\text{e-}016$  and

$$IO = \begin{bmatrix} 0.5 & 8.1685\text{e-}017 & 5.8467\text{e-}017 \\ 8.1685\text{e-}017 & 0.5 & 2.4303\text{e-}016 \\ 5.8467\text{e-}017 & 2.4303\text{e-}016 & 0.5 \end{bmatrix}$$

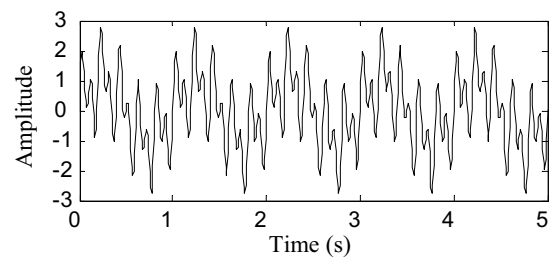


Figure 1. Time history curve of a simple signal

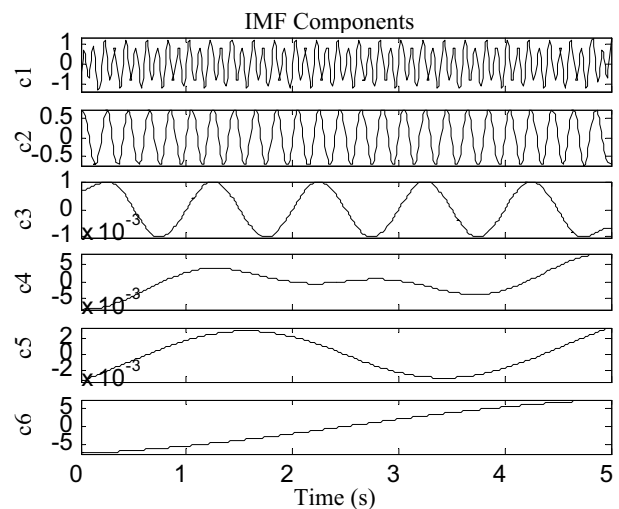


Figure 2. The original IMF components (EMD)

<sup>a</sup> Corresponding author: [lml@tongji.edu.cn](mailto:lml@tongji.edu.cn), 13701910214@163.com

The signal  $X(t)$  can be decomposed as five IFMs and one residual function when applying the EMD, shown in Figure 2. These five IFMs are defined as original IFMs.

The orthogonal index  $IOT = 0.06633$  and  $IO_{jk}$  are shown in Table 1. Comparing with the orthogonal level of three sinusoidal components, the orthogonal level of the original IFMs drops a lot.

**Table 1.** The values of the orthogonal index  $IO_{jk}$  (original IFMs)

Order $j,k$	1	2	3	4	5
1	0.5	1.1E-01	3.9E-03	8.9E-05	3.2E-05
2	1.1E-01	0.5	4.9E-02	2.1E-04	8.6E-05
3	3.9E-03	4.9E-02	0.5	1.5E-03	5.2E-04
4	8.9E-05	2.1E-04	1.5E-03	0.5	3.0E-01
5	3.2E-05	8.6E-05	5.2E-04	3.0E-01	0.5

## 2 Orthogonal technique for original IFMs

Gram-Schmidt method is applied usually for obtaining the orthogonal eigenvectors or Ritz vectors in structural dynamics<sup>[4]</sup>. This method is used here to achieve the orthogonal IFMs from the original IFMs. The process to obtain the orthogonal IFMs is defined as improved EMD (IEMD). There are three different ways to get the orthogonal IFMs  $c_j^*(t)$  from the original IFMs  $c_j(t)$ . The signal  $X(t)$  is expressed by the orthogonal IFMs as

$$X(t) = \sum_{j=1}^n c_j^*(t) + r_n(t) \quad (5)$$

### 2.1 Forward sequence orthogonalization

The original IFMs obtained from Eq.(1) are sequenced from high frequency to low frequency. In Gram-Schmidt orthogonalization, the sequence order is not changed. The computing steps of the orthogonalization are introduced as follows<sup>[5]</sup>.

(1) The first basic orthogonal function is taken as the first original IMF, that is

$$d_1(t) = c_1(t) \quad (6)$$

(2) The second basic orthogonal function is formed from the second original IMF  $c_2(t)$ , but orthogonal to the first basic function  $d_1(t)$ .

$$d_2(t) = c_2(t) - \beta_{21}d_1(t) \quad (7)$$

in which  $\beta_{21}$  is defined as the orthogonal factor between  $c_2(t)$  and  $d_1(t)$  and obtained from

$$\int_0^T d_1(t)d_2(t)dt = \int_0^T c_2(t)d_1(t)dt - \beta_{21}\int_0^T d_1^2(t)dt = 0$$

$$\beta_{21} = \frac{\int_0^T c_2(t)d_1(t)dt}{\int_0^T d_1^2(t)dt} \quad (8)$$

(3) Recurrent formula for solving high order basic orthogonal functions,

$$d_{j+1}(t) = c_{j+1}(t) - \sum_{i=1}^j \beta_{j+1,i}d_i(t) \quad (9)$$

Utilizing the orthogonality of the first  $j$  basic orthogonal functions and equation

$$\int_0^T d_{j+1}(t)d_k(t)dt = \int_0^T c_{j+1}(t)d_k(t)dt - \sum_{i=1}^j \beta_{j+1,i} \int_0^T d_k(t)d_i(t)dt = 0 \quad (10)$$

when  $k=i$ , we can obtain

$$\beta_{j+1,i} = \frac{\int_0^T c_{j+1}(t)d_i(t)dt}{\int_0^T d_i^2(t)dt} \quad (11)$$

(4) Substitute Eqs.(6), (7) and (9) into Eq. (1), the signal  $X(t)$  can be described as

$$X(t) = c_1^*(t) + c_2^*(t) + c_3^*(t) + \dots + c_j^*(t) + \dots + c_{n-1}^*(t) + c_n^*(t) + r_n(t)$$

$$= \sum_{j=1}^n c_j^*(t) + r_n(t) = \sum_{j=1}^n a_j d_j(t) + r_n(t) \quad (12)$$

where  $a_j = \sum_{i=j}^n \beta_{i,j}$  ( $j = 1, 2, \dots, n$ ),  $\beta_{i,j} = 1 (i = j)$ .  $c_j^*(t)$

is the  $j^{\text{th}}$  orthogonal IMF that are sequenced from high frequency to low frequency.

### 2.2 Backward sequence orthogonalization

In Gram-Schmidt orthogonalization, the sequence order is changed reversely. It means that the computing steps are modified as follows.

(1) The first basic orthogonal function is taken as the last original IMF, that is

$$d_1(t) = c_n(t) \quad (13)$$

(2) The second basic orthogonal function is formed from the last second original IMF  $c_{n-1}(t)$ , but orthogonal to the first basic function  $d_1(t)$ .

$$d_2(t) = c_{n-1}(t) - \beta_{21}d_1(t) \quad (14)$$

in which  $\beta_{21}$  is defined as the orthogonal factor between  $c_{n-1}(t)$  and  $d_1(t)$  and obtained from

$$\beta_{21} = \frac{\int_0^T c_{n-1}(t)d_1(t)dt}{\int_0^T d_1^2(t)dt} \quad (15)$$

(3) Recurrent formula for solving high order basic orthogonal functions,

$$d_{j+1}(t) = c_{n-j}(t) - \sum_{i=1}^j \beta_{j+1,i}d_i(t) \quad (16)$$

$$\beta_{j+1,i} = \frac{\int_0^T c_{n-j}(t)d_i(t)dt}{\int_0^T d_i^2(t)dt} \quad (17)$$

(4) Substitute Eqs.(13), (14) and (16) into Eq. (1), the signal  $X(t)$  can also be described by Eq. (12). However, the difference is that the orthogonal IFMs  $c_j^*(t)$  are sequenced from low frequency to high frequency.

Obviously, if the work of rearranging reversely the sequence order of the original IMFs is finished at first, the orthogonal computations can be completed by Eqs. (6)-(12).

### 2.3 Arbitrary sequence orthogonalization

In Gram-Schmidt orthogonalization, the sequence order is changed arbitrarily. It means that any one of these  $n$  orthogonal IMFs can be selected as the first basic orthogonal function and the sequence order of these  $n$  original IMFs can be rearranged if necessary. After the sequence order rearrangement, the computing steps of the Gram-Schmidt orthogonalization are the same introduced in section 2.1. The difference is that the orthogonal IMFs  $c_j^*(t)$  are not sequenced from low frequency to high frequency or from high frequency to low frequency.

## 3 Numerical example

The signal  $X(t)$  shown in Eq.(4) is continuously used as the example. The comparisons of the numerical results obtained from different orthogonal methods are shown as follows. In arbitrary sequence method, the 3<sup>th</sup> original IMF is selected as the first basic orthogonal IMF. The following is the 2<sup>nd</sup>, the 1<sup>st</sup>, the 4<sup>th</sup> and 5<sup>th</sup> IMF.

### 3.1. Orthogonal IMF components

The orthogonal IMFs are shown in Figures (3)-(5).

### 3.2 Orthogonal index

The values of integral orthogonal index  $IOT$  are 0.000504 (IEMD-1), 0.000613 (IEMD-2) and 0.000452 (IEMD-3) respectively. The values of the orthogonal index  $IO_{jk}$  are listed in Tables 2-4.

It is obvious that the orthogonal level of the IMFs has been greatly improved when the orthogonal technique is applied to the original IMFs.

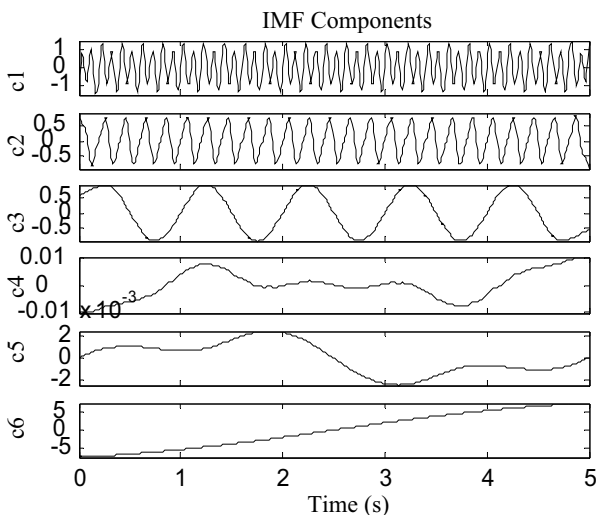


Figure 3. The orthogonal IMF components (IEMD-1)

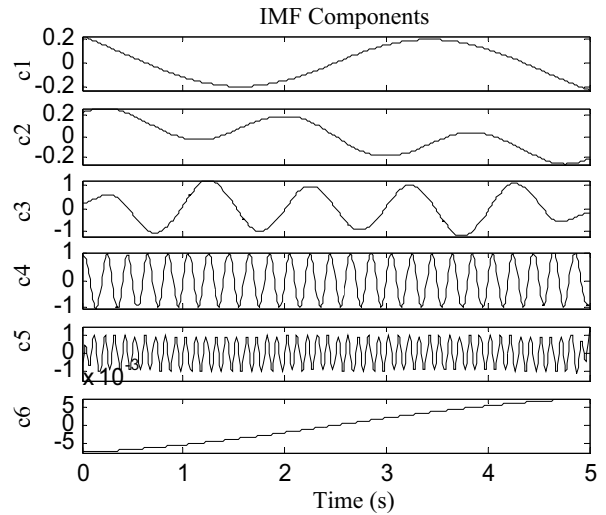


Figure 4. The orthogonal IMF components (IEMD-2)

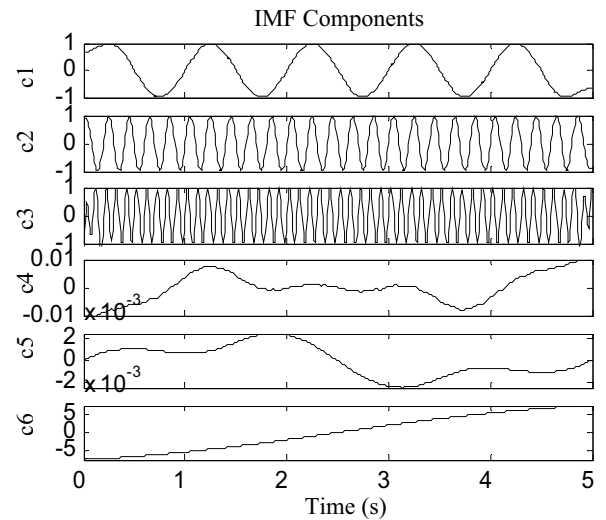


Figure 5. The orthogonal IMF components (IEMD-3)

Table 2. The values of the orthogonal index  $IO_{jk}$  (IEMD -1)

Order $j,k$	1	2	3	4	5
1	0.5	3.2E-17	2.7E-18	4.4E-20	8.5E-21
2	3.2E-17	0.5	8.2E-18	3.1E-19	5.2E-20
3	2.7E-18	8.2E-18	0.5	1.3E-18	1.2E-19
4	4.4E-20	3.1E-19	1.3E-18	0.5	3.2E-16
5	8.5E-21	5.2E-20	1.2E-19	3.2E-16	0.5

Table 3. The values of the orthogonal index  $IO_{jk}$  (IEMD -2)

Order $j,k$	1	2	3	4	5
1	0.5	2.3E-18	1.8E-17	2.9E-18	2.1E-18
2	2.3E-18	0.5	3.6E-17	2.5E-18	1.1E-18
3	1.8E-17	3.6E-17	0.5	8.4E-18	9.0E-19
4	2.9E-18	2.5E-18	8.4E-18	0.5	7.2E-17
5	2.1E-18	1.1E-18	9.0E-19	7.2E-17	0.5

**Table 4.** The values of the orthogonal index  $IO_{jk}$  (IEMD -3)

Order $j,k$	1	2	3	4	5
1	0.5	4.5E-18	4.8E-18	1.8E-18	8.0E-20
2	4.5E-18	0.5	8.6E-17	1.6E-19	3.8E-20
3	4.8E-18	8.6E-17	0.5	3.3E-19	3.6E-20
4	1.8E-18	1.6E-19	3.3E-19	0.5	1.6E-16
5	8.0E-20	3.8E-20	3.6E-20	1.6E-16	0.5

### 3.3 Importance of orthogonality

The orthogonality of the IMFs has an important effect on its applications. It is illustrated by a simple example. If the signal  $X(t)$  is a seismic wave, its vibrating energy can be computed by

$$E_x = \int_0^T X^2(t) dt \quad (18)$$

The energy of each component in the seismic wave can be expressed

$$E_j = \int_0^T c_j^2(t) dt \quad (j=1, \dots, n+1) \quad (19)$$

If the wave components are orthogonal, there are

$$E_{tot} = \sum_{j=1}^{n+1} E_j = E_x \quad (20)$$

$$E_{jk} = \int_0^T c_j(t)c_k(t) dt = 0 \quad (j, k=1, \dots, n+1; j \neq k) \quad (21)$$

Now we compute the energy of the signal composed by three sinusoidal waves shown in Eq.(4). Total energy

$E_{tot} = 750$  and the energy between the sinusoidal components is listed in the following matrix. Its total energy is equal to the sum of three component energy. The numerical results satisfy Eqs. (20) and (21) as the sinusoidal functions are orthogonal.

$$E = \begin{bmatrix} 250 & -4.08e-014 & 2.92e-014 \\ -4.08e-014 & 250 & 1.22e-013 \\ 2.92e-014 & 1.22e-013 & 250 \end{bmatrix}$$

When the signal  $X(t)$  is decomposed by EMD and improved EMD respectively, the values of its  $E_{tot}$  and  $E_j$  are listed in Table 5. It can be seen from numerical results in Table 5 that total energy of the signal  $X(t)$  in EMD method is underestimated as the IMFs are not orthogonal that causes energy leakage between the components. Three IEMD methods improve the situation and ensure high calculation accuracy for total energy of the signal. However, the calculation accuracy of component energy is different for three IEMD methods. IEMD-3 is the best to get good results. This is the problem to be paid attention to.

### 4 Conclusion

The improved empirical mode decomposition has been developed to obtain the orthogonal intrinsic mode function. The numerical results show that the method has good calculation accuracy.

**Table 5.** The values of total energy and component energy

Method	$E_x$	$E_1$	$E_2$	$E_3$	$E_4$	$E_5$	$E_6$	$E_{tot}$	Error(%)
EMD	750	<b>265.84</b>	<b>136.65</b>	<b>259.76</b>	0.0076	0.002	0.0119	662.28	-11.7
IEMD-1		<b>358.39</b>	<b>133.58</b>	<b>258.65</b>	0.0134	0.0009	0.0119	750.64	0.09
IEMD-2		8.8587	11.52	<b>238.12</b>	<b>241.14</b>	<b>250.99</b>	0.0119	750.64	0.09
IEMD-3		<b>258.49</b>	<b>240.93</b>	<b>251.19</b>	0.0134	0.0009	0.0119	750.64	0.09

### References

1. N.E. Huang, S.R. Long, Proc. R. Soc. Lond. A, **454**, 903-995 (1998)
2. Y.L. Xu, J. Chen, J. of Engineering Mechanics, **130**, 1279-1288 (2004)

3. R. Zhang, S. Ma, E. Safak, S. Hartzell, J. of Engineering Mechanics, **129**, 861-875 (2003)
4. R.W. Clough, J. Penzien, *Dynamics of structures* ( McGraw-Hill, Inc, New York, 1993)
5. M. Lou, T. Huang, J. of Tongji Universty, **35**, 293-298 (2007) (in Chinese)