

# New single crystal superalloys – overview and update

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**Abstract.** Single crystal (SX) superalloys have wide application in the high pressure turbine section of aero and industrial gas turbine engines due to the unique combination of properties and performance. Since introduction of single crystal casting technology, SX alloy development has focused on increased temperature capability, and major improvements in alloy performance have been associated with the introduction of new alloying elements, including rhenium (Re) and ruthenium (Ru). 3% Re-containing second generation alloys have seen the greatest market utilization and have become the benchmark alloys for comparing new alloy developments. However, Re and Ru are rare elements with limited production/availability and corresponding high costs. This has resulted in significant escalation of SX alloy costs, resulting in much interest in the development of improved SX superalloys with lower Re or no Re content compared to second generation alloys. Cannon-Muskegon<sup>®</sup> has developed two new SX superalloys: 1.5% Re CMSX<sup>®</sup>-8 alloy and CMSX<sup>®</sup>-7 alloy, which contains no Re, as alternatives to first and second generation alloys for applications which require slightly less ultra high temperature capability compared to current alloys. This paper provides an overview of development and characterization of these SX alloys, including an update on recent results.

## 1. Introduction

Since the introduction of single crystal (SX) casting technology in the late 1970's, single crystal alloy development has generally focused on increasing temperature capability. Major improvements in alloy performance have been associated with the introduction of new alloying elements, including rhenium (Re) and ruthenium (Ru) [1,2]. Rhenium, in particular, has been widely used in advanced single crystal superalloys for turbine blade, vane and seal segments due to its potent effect in slowing diffusion, creep deformation and fatigue crack initiation under high temperature operating conditions [3]. High temperature creep resistance and fatigue properties are directly related to the useful service life of gas turbine components and turbine engine performance such as power output, fuel burn and carbon dioxide emissions. Consequently, 3% Re-containing “second generation” SX alloys, such as CMSX-4<sup>®</sup>, PWA 1484 and Rene' N5 have seen the greatest market utilization and have become the benchmark alloys for comparing new alloy developments.

However, Re is a rare element by-product from mining and processing copper and copper/molybdenum; Ru is a precious metal by-product principally from platinum production. As a result, both elements have limited market availability and extremely high cost which has resulted in significant escalation of SX alloy costs. In addition, Re use creates a supply chain risk economically and

**Table 1.** CMSX-8 alloy nominal chemistry.

Element	Wt%	Element	Wt%
Cr	5.4	Re	1.5
Co	10	Al	5.7
Mo	0.6	Ti	0.7
Ta	8	Hf	0.1
W	8	Ni	Balance

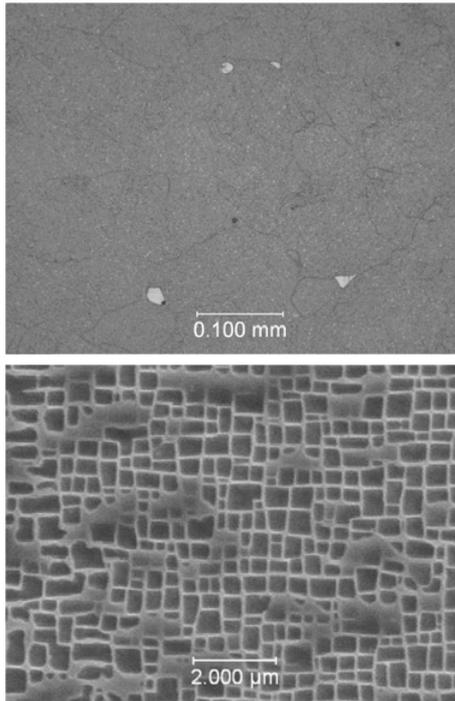
strategically. Consequently, industry interest in alternative SX superalloys with reduced Re content has emerged.

As initially presented at SUPERALLOYS 2012 [4], Cannon-Muskegon has developed two new proprietary SX superalloys: CMSX<sup>®</sup>-8 alloy containing 1.5% Re is an alternative to 2<sup>nd</sup> generation alloys for applications with slightly lower maximum temperature requirements and CMSX<sup>®</sup>-7 alloy, which contains no Re, with improved properties over 1<sup>st</sup> generation alloys, such as CMSX-2/3<sup>®</sup> and PWA 1480.

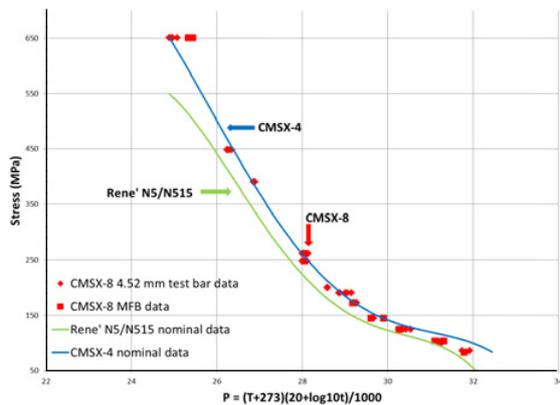
## 2. CMSX-8 alloy

The nominal chemistry of CMSX-8 alloy is shown in Table 1. Development goals were to target 2<sup>nd</sup> generation SX alloy properties, castability and stability with significantly reduced Re content. Refractory elements (Ta, W, Re, Mo) were balanced to achieve creep-rupture properties and balanced with Cr and Co content to ensure phase stability. The high Ta content is designed for SX castability and freedom from freckling defects. Al, Ti and Ta content will produce ~70% volume fraction  $\gamma'$  phase, while high Al, low Mo plus a small Hf addition

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**Figure 1.** CMSX-8 casting microstructure following solution + double age heat treatment.



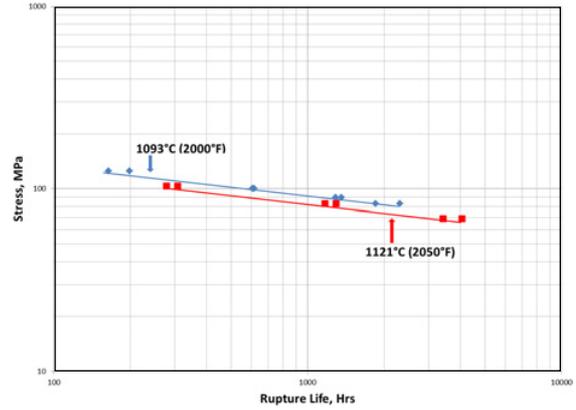
**Figure 2.** Larson-Miller rupture life of CMSX-8 vs. CMSX-4 and Rene' N5/N515.

improves bare alloy oxidation resistance and coating adherence. The density of CMSX-8 alloy is  $\sim 8.85 \text{ g/cm}^3$ . DSC solidus and liquidus temperatures are  $1338^\circ\text{C}$  and  $1389^\circ\text{C}$ , respectively.

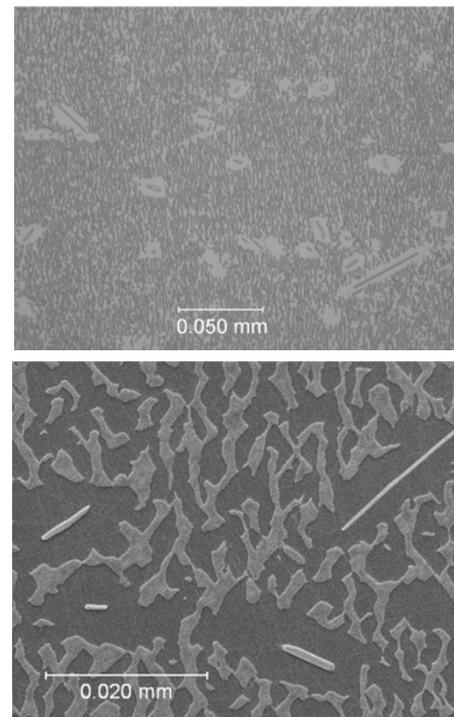
Development of a multi-step solution heat treatment and double age cycle produces complete  $\gamma'$  solutioning with some remnant  $\gamma/\gamma'$  eutectic, no incipient melting and  $\sim 0.45\mu\text{m}$  average cubic aligned  $\gamma'$  phase indicating appropriate  $\gamma/\gamma'$  mismatch and interfacial chemistry (Fig. 1).

### 2.1. Mechanical properties

Extensive mechanical property testing has been conducted on CMSX-8 alloy, including creep- and stress-rupture testing over a range of temperature/stress conditions. As shown in Larson-Miller rupture life curves, CMSX-8 alloy has similar creep properties to CMSX-4 alloy to



**Figure 3.** CMSX-8 alloy stress-rupture curves.



**Figure 4.** CMSX-8 microstructure following 4060 hours stress-rupture testing at  $1121^\circ\text{C}$ .

approximately  $1038^\circ\text{C}$  and exceeds published properties for Rene' N5 and Rene' N515 alloys over a range of test conditions (Fig. 2) [1,5,6]. Stress-rupture curves at  $1093^\circ\text{C}$  and  $1121^\circ\text{C}$  are linear indicating no fall-off in properties due to phase stability issues (Fig. 3). This is confirmed by post-test metallography after 4060 hours at  $1121^\circ\text{C}$  which shows small isolated TCP phase formation, but not associated with creep cracking or significant de-alloying (Fig. 4).

Fatigue properties are typically design-specific to each engine manufacturer; however, limited strain-controlled low cycle fatigue (LCF) testing has been conducted in conjunction with two OEMs for comparison to commercial SX alloy applications. Typical S-N curves for R-ratios of 0 and  $-1$  are shown in Figs. 5–7. Based on discussions with the OEM, results obtained are excellent compared to CMSX-4 alloy.

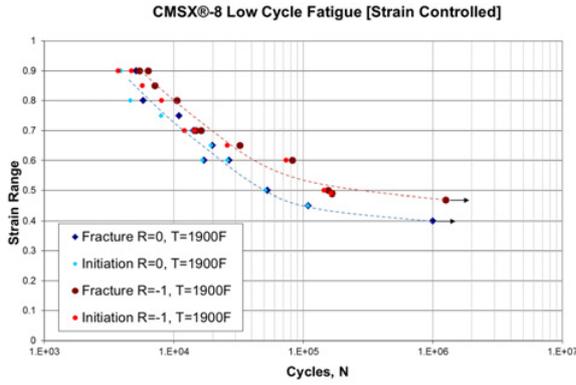


Figure 5. CMSX-8 1038 °C LCF data.

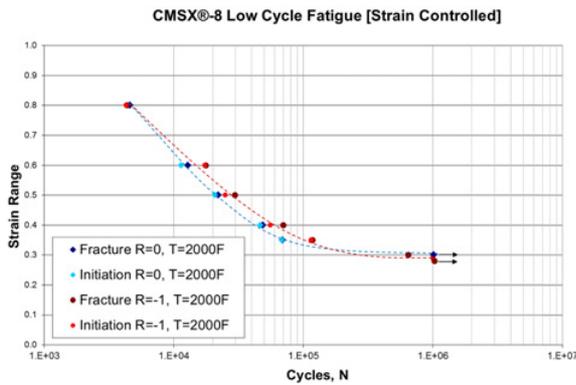


Figure 6. CMSX-8 1093 °C LCF data.

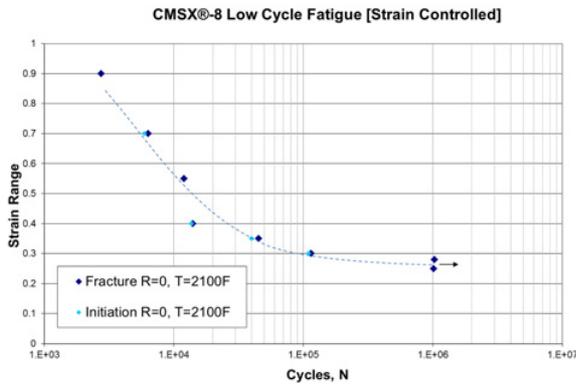


Figure 7. HIP'ed CMSX-8 1150 °C LCF data.

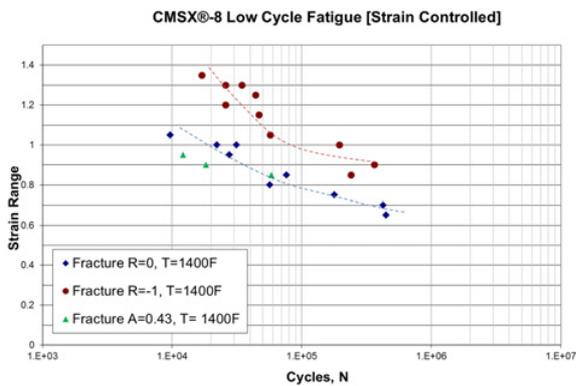


Figure 8. CMSX-8 760 °C LCF data.

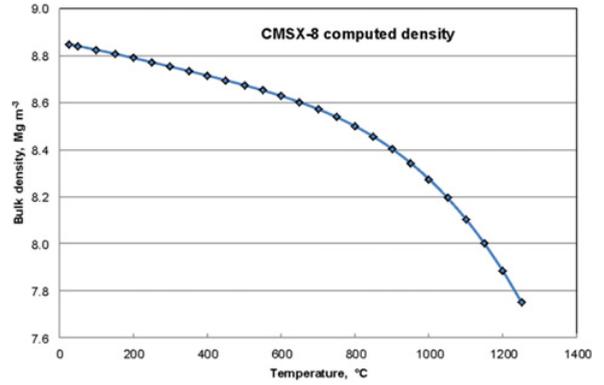


Figure 9. CMSX-8 density vs. Temperature.

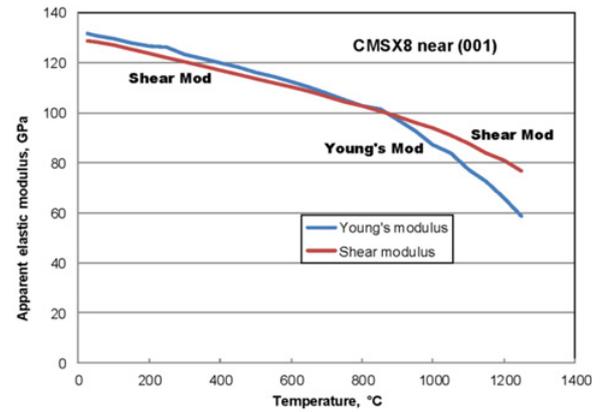


Figure 10. Young's and shear modulus vs. Temperature.

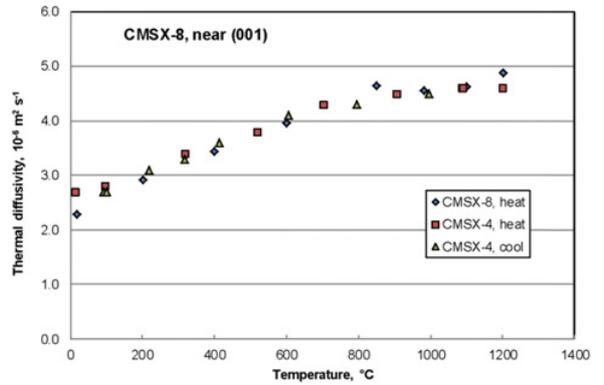


Figure 11. Thermal diffusivity vs. Temperature.

Similar testing was conducted at 760 °C, with R-ratios of -1, 0 and 0.4, approximating the temperature/stress regime for the blade shank area for commercial turbine blade applications (Fig. 8). This data indicated favourable performance compared to the current 1<sup>st</sup> generation (non-Re-bearing) SX alloy.

## 2.2. Physical properties

CMSX-8 physical properties have been characterized in collaboration with the National Physical Laboratory in the United Kingdom. Density, Young's and shear moduli, thermal diffusivity and thermal conductivity as a function

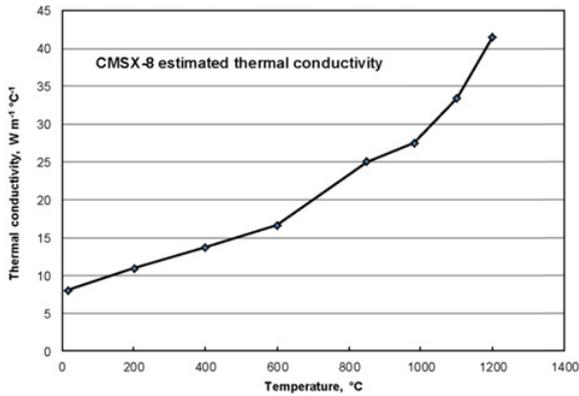


Figure 12. Thermal conductivity vs. temperature.

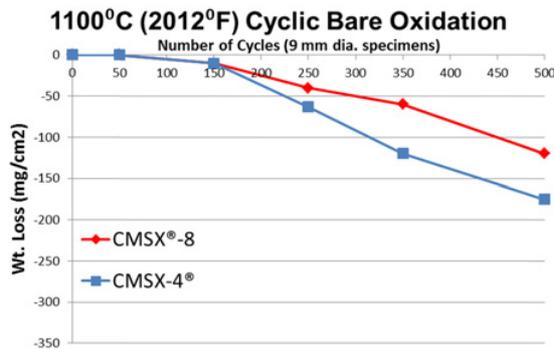


Figure 13. CMSX-8 vs. CMSX-4 bare oxidation comparison.

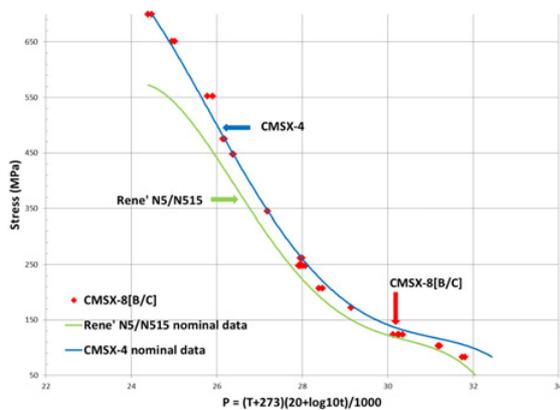


Figure 14. Larson-Miller rupture life of CMSX-8[B/C] alloy vs. CMSX-4 and Rene' N5/N515.

of temperature are shown in Figs. 9–12. Initial cyclic bare oxidation test results, conducted by Turbomeca at 1100 °C are shown in Fig. 13.

### 2.3. Alloy modifications and enhancements

The addition of grain boundary strengthening elements carbon and boron have been shown to improve low angle boundary (LAB) defect accommodation for large and/or difficult to cast SX components such as industrial gas turbine blades and vanes [7]. Assessment of the modified alloy CMSX-8[B/C] is well underway and show creep-rupture properties consistent with the standard CMSX-8 database (Fig. 14).

Table 2. CMSX-7 alloy nominal chemistry.

Element	Wt%	Element	Wt%
Cr	6	Re	–
Co	10	Al	5.7
Mo	0.6	Ti	0.8
Ta	9	Hf	0.2
W	9	Ni	Balance

Proprietary Cannon-Muskegon virgin raw material and vacuum induction melting technology is also available to produce CMSX-8(SLS) and CMSX-8[B/C](SLS) alloys with extremely low sulphur content. These alloys demonstrate the same alloys properties with improved environmental properties (oxidation/hot corrosion) for enhanced performance and TBC/coating life.

### 2.4. Pre-production experience

Pre-production casting and design database property assessment is in process at two OEM's and multiple major SX casting foundries for both CMSX-8 and CMSX-8[B/C] alloys. The CMSX-8[B/C] work involves very large SX IGT 1<sup>st</sup> stage blades with mould pour weights of approximately 55 kgs. This work confirms the excellent castability/yield results, mechanical and physical properties established during alloy development; the heat qualification properties exceed preliminary specification stress-rupture requirements by more than 2x.

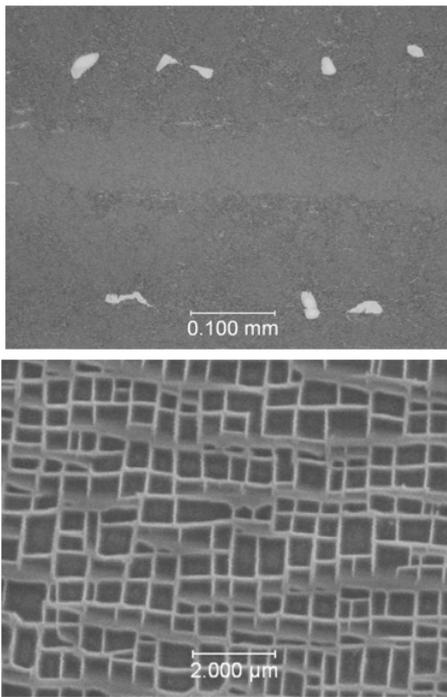
### 3. CMSX-7 alloy

In a parallel effort, development of a new non-Re-bearing alloy with improved mechanical properties compared to existing 1<sup>st</sup> generation alloys was undertaken and produced CMSX-7 alloy (Table 2). This work utilized 30+ years industry experience and understanding of SX casting alloys and technology to further optimize strength, heat treatment window, castability, stability and oxidation performance. The alloy employs a balance of refractory elements (Ta, Mo and W) for creep-rupture strength; Cr and Co adjustments for stability; and high Ta for castability. Al, Ti and Ta content targets ~70% volume fraction  $\gamma'$  phase; and high Al, low Mo plus small Hf addition results in good bare oxidation resistance and coating adherence. The density of CMSX-7 alloy is approximately 8.8 g/cm<sup>3</sup>. DSC solidus and liquidus are 1325 °C and 1381 °C, respectively.

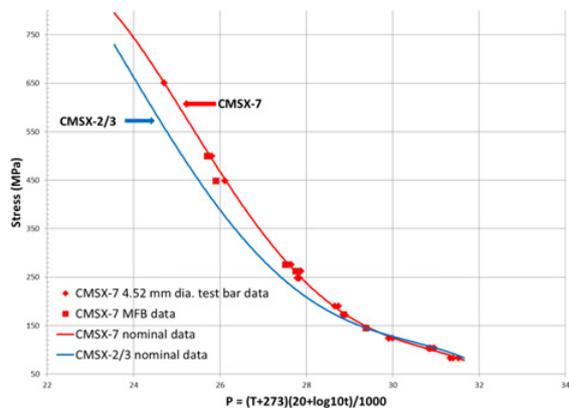
A multi-step solution heat treatment and double age cycle produces complete  $\gamma'$  solutioning with some remnant  $\gamma/\gamma'$  eutectic, no incipient melting and ~0.5  $\mu\text{m}$  average cubic aligned  $\gamma'$  phase indicating appropriate mismatch and interfacial chemistry (Fig. 15).

#### 3.1. Mechanical properties

Mechanical property characterization of CMSX-7 alloy includes creep- and stress-rupture testing across a matrix of temperature/stress conditions and strain-controlled low cycle fatigue testing. Larson-Miller rupture life of CMSX-7 alloy compared to CMSX-2/3 demonstrates improved properties to ~1038 °C and similar properties above (Fig. 16) [8]. Surprisingly, CMSX-7 alloy



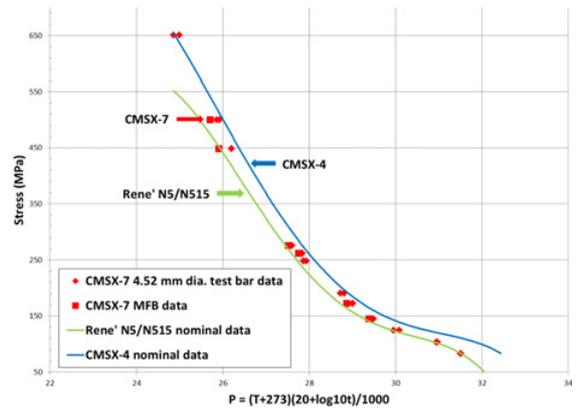
**Figure 15.** CMSX-7 casting microstructure following solution + double age heat treatment.



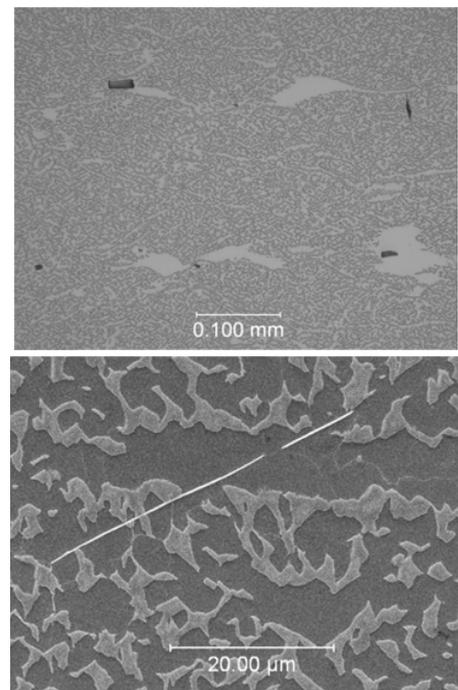
**Figure 16.** Larson-Miller rupture life of CMSX-7 vs. CMSX-2/3.

rupture life is similar to Rene' N5/N515 alloy data despite the absence of Re in CMSX-7 (Fig. 17) [1,5,6]. This improvement in strength is attributed to the significant increase in refractory content, Ta+W+Mo ~18.6%, compared to 14.6% for CMSX-2/3, 16.5% for CMSX-4 and 16% for Rene' N5 alloys. CMSX-7 alloy accommodates the higher refractory content through appropriate reduction of Cr content to mitigate stability problems. This is depicted in post-creep-rupture metallography (Fig. 18), which shows typical rafted microstructure with minimal non-detrimental TCP phase formation.

Results from strain-controlled LCF testing of CMSX-7 alloy are shown in S-N curves at 1038 °C and 1093 °C (Fig. 19). Of note, crack initiation data at 1038 °C is surprisingly good, similar to CMSX-4 data for HIP'ed + heat treated specimens [9].



**Figure 17.** Larson-Miller rupture life of CMSX-7 vs. CMSX-4 and Rene' N5/N515.



**Figure 18.** CMSX-7 microstructure following 1176 hours stress-rupture testing at 1093 °C.

### 3.2. Castability

SX castability assessments for CMSX-7 alloy have been excellent with 95%+ yield for primary orientation (within 10° of <001> for seeded casting) and grain defects on test material.

## 4. Summary

Two new single crystal alloys, low Re CMSX-8 and CMSX-7 containing no Re, offer competitive properties to existing commercial SX alloys with lower alloy cost. CMSX-8 alloy is comparable to CMSX-4 alloy in terms of creep-and stress-rupture properties to at least 1010 °C with attractive LCF performance. CMSX-7 alloy demonstrates improved properties over commercial 1<sup>st</sup> generation SX alloys and is remarkably competitive with Re-containing alloys Rene' N5/N515.

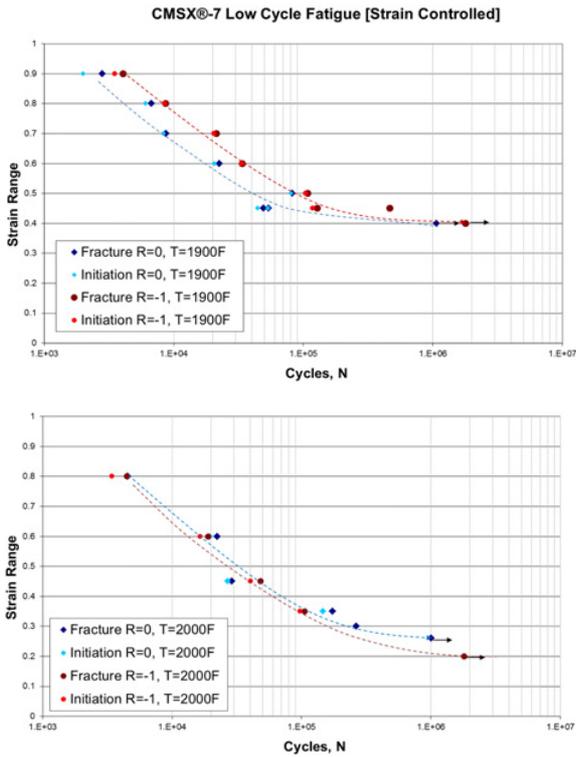


Figure 19. CMSX-7 1038 °C and 1093 °C LCF data.

Both alloys have demonstrated excellent castability and phase stability. Alloy modifications for enhanced oxidation resistance/TBC life and improved grain defect accommodation for large and/or complex castings are also available.

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